

# Programa Oficial de Posgrado en INGENIERIA MECÁNICA y de MATERIALES

# MASTER EN SISTEMAS MECÁNICOS

# **ANEXOS**

# RETROFIT DE UNA MAQUINA DE ENSAYOS DE RODADURA A DOS FLANCOS PARA ENGRANAJES SINFÍN CORONA

Autor

Marcos Pueo Arteta

Director

Jorge Santolaria Mazo

Departamento de Ingeniería de Diseño y Fabricación Escuela de Ingeniería y Arquitectura

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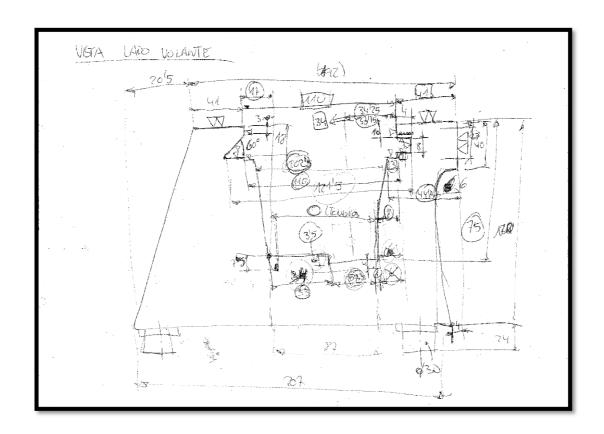
## **ANEXO I: CROQUIS**

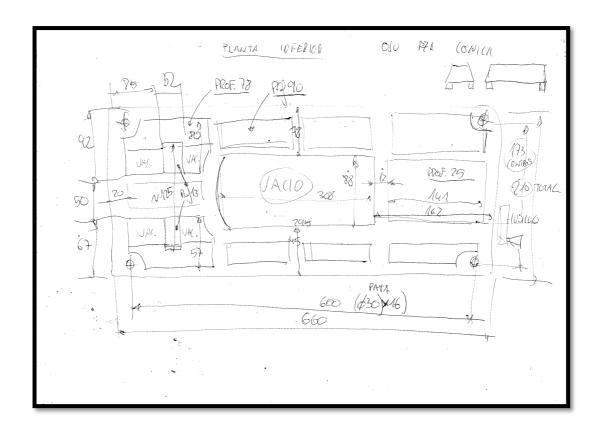
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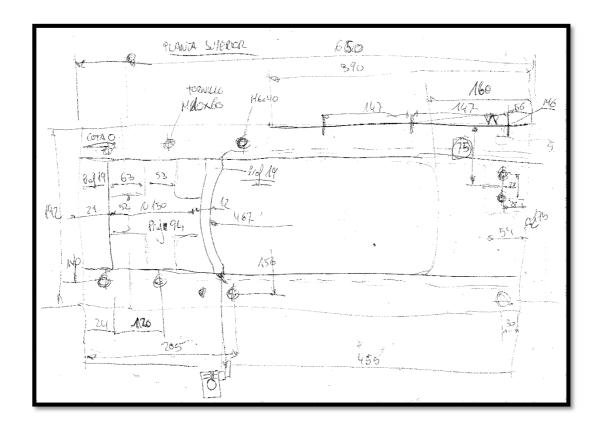
Los croquis que podemos encontrar son los siguientes:

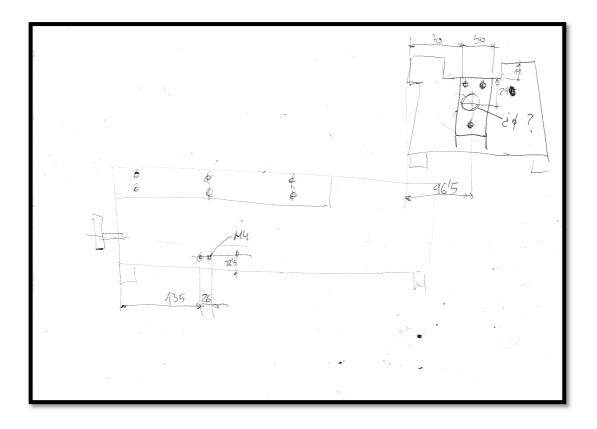
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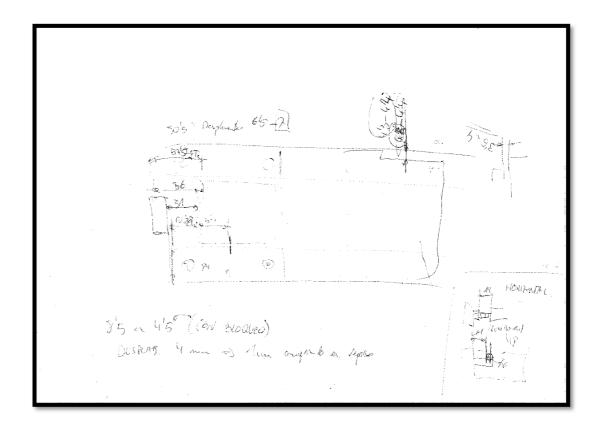
Croquis 1 <u>Bancada</u>



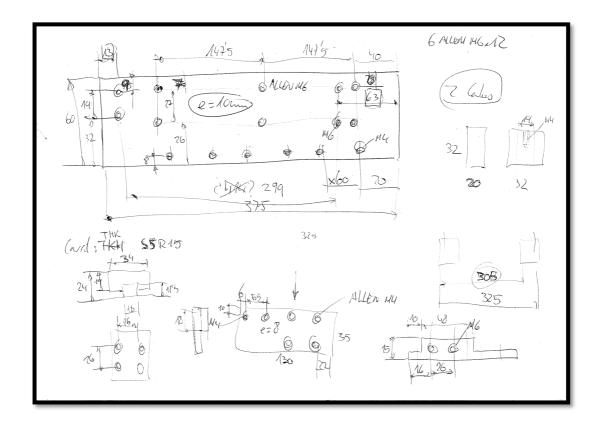


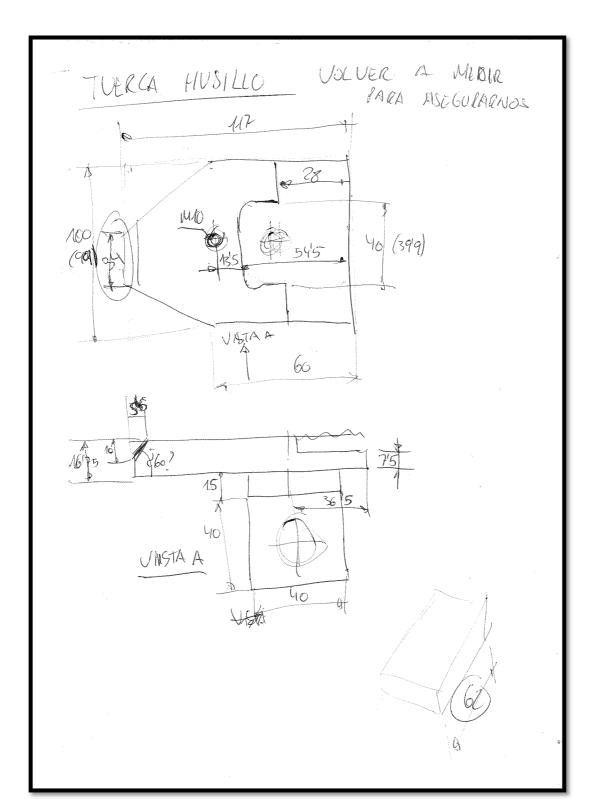




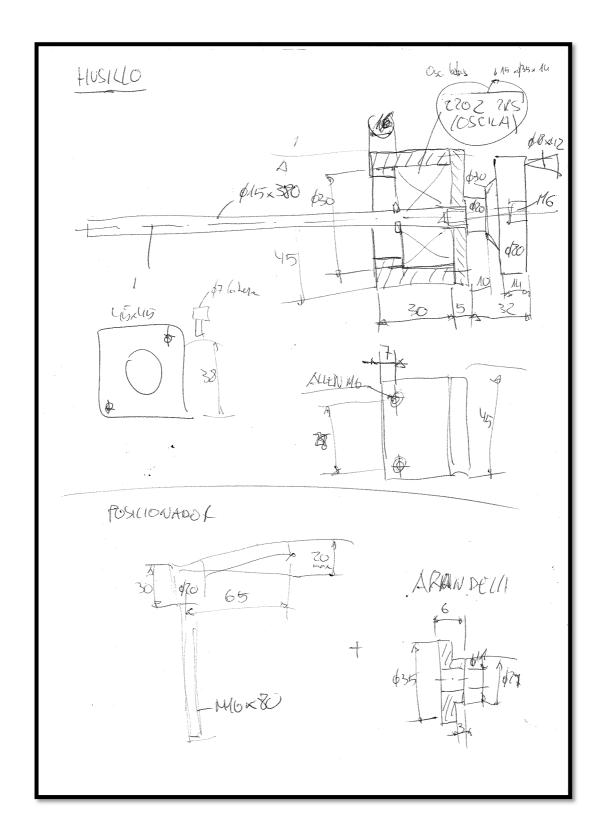


Croquis 2 <u>Sistema encoder lineal</u>

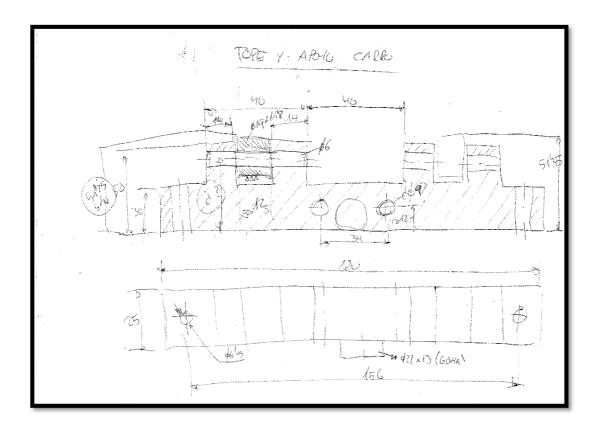




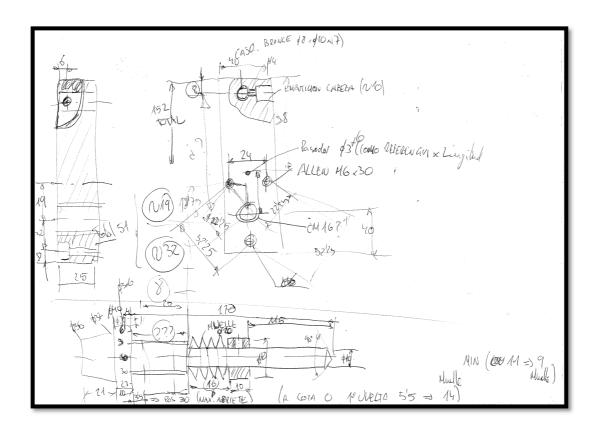
Croquis 3 <u>Sistema de posicionamiento carro porta-sinfín</u>



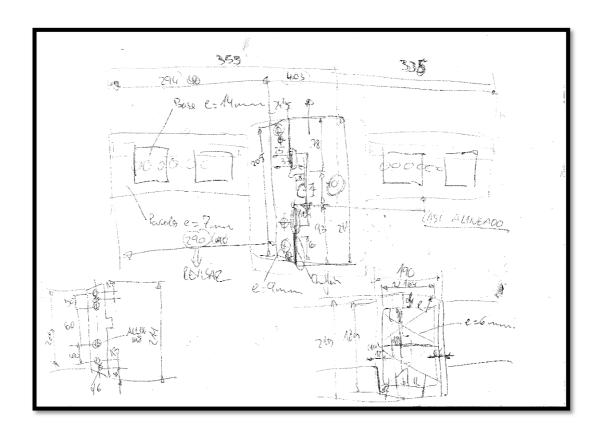
Croquis 4 <u>Tope mecánico carro porta-sinfín</u>

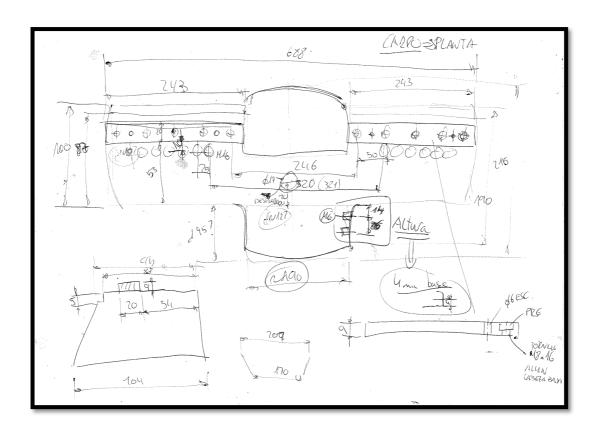


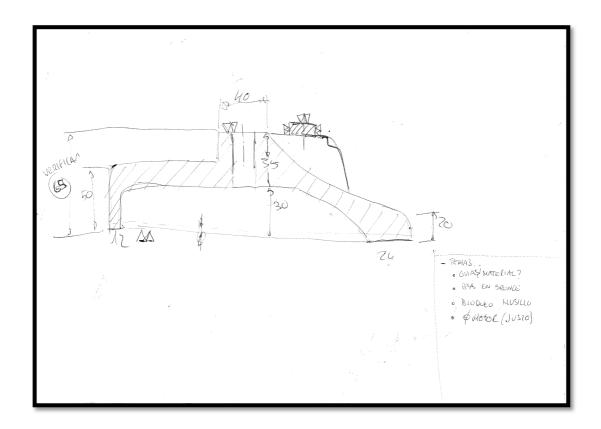
Croquis 5 <u>Sistema regulación presión muelle columna</u>



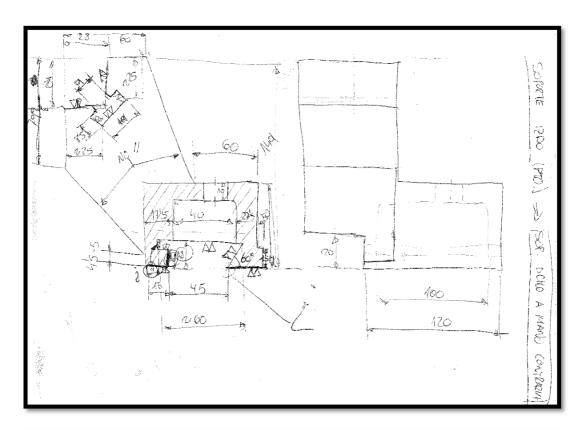
Croquis 6 <u>Base carro porta-sinfín</u>

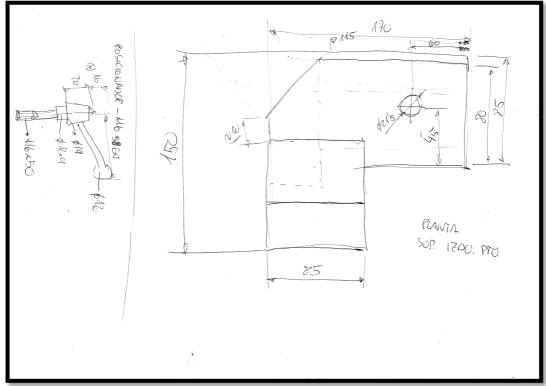




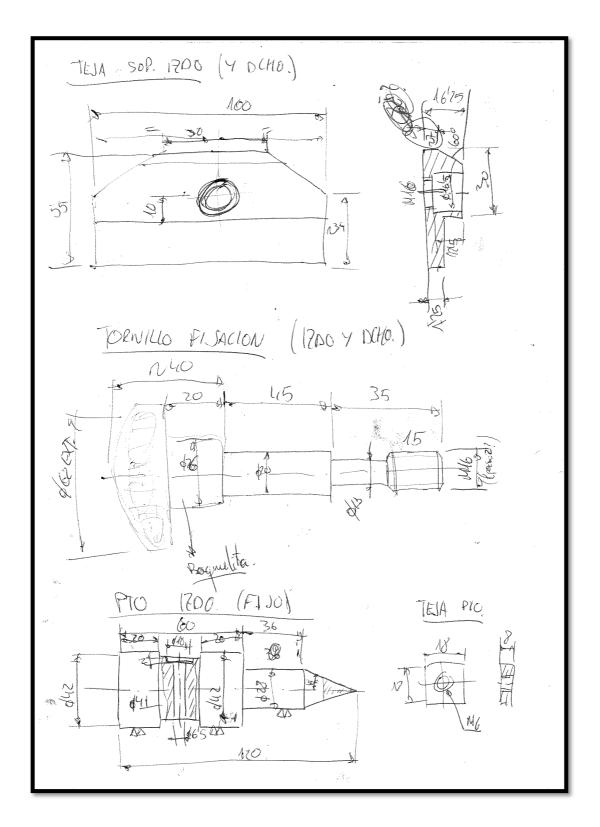


Croquis 7 Porta puntos

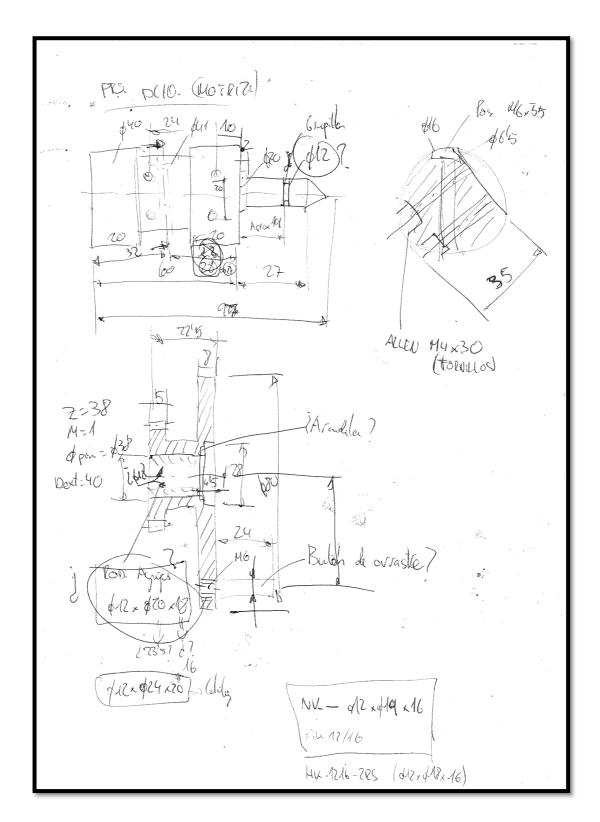




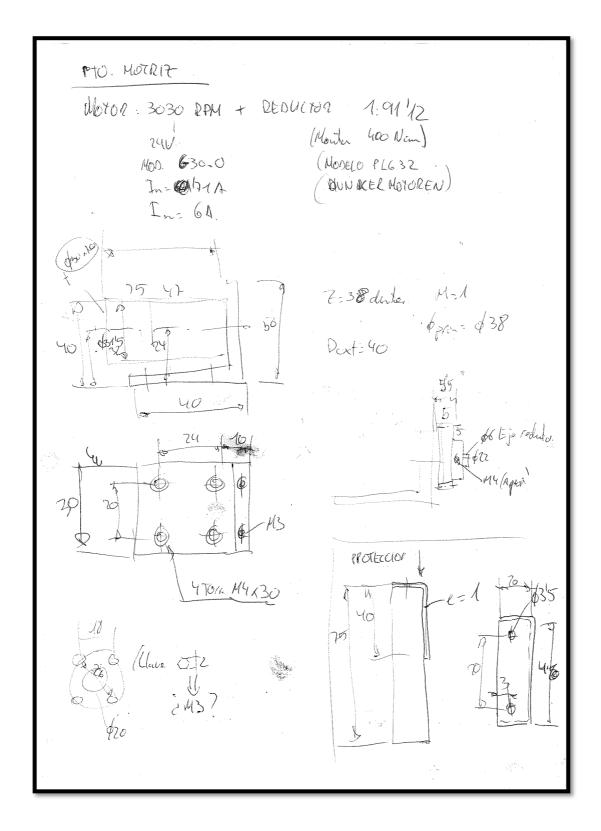
Croquis 8 Punto fijo y maneta posicionadora



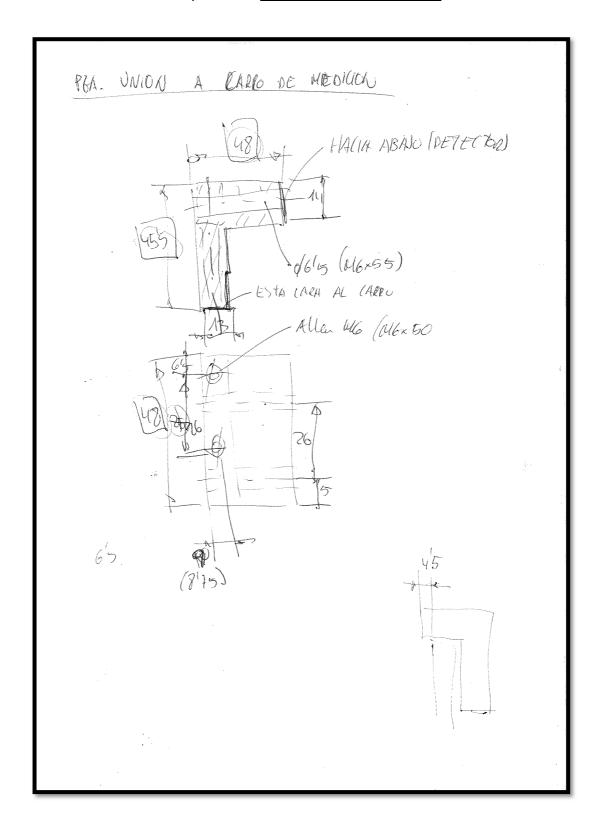
Croquis 9 Punto motriz



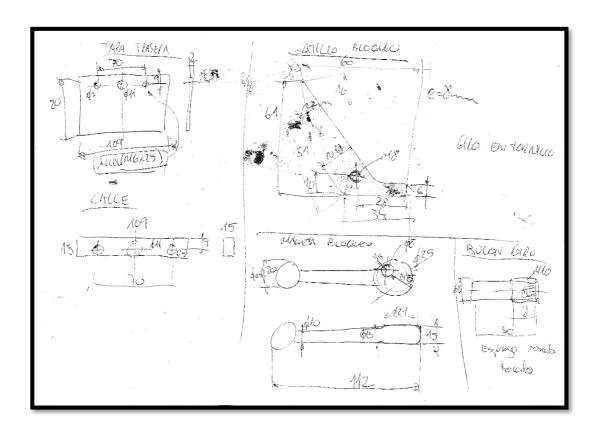
Croquis 10 Soporte y protección punto motriz



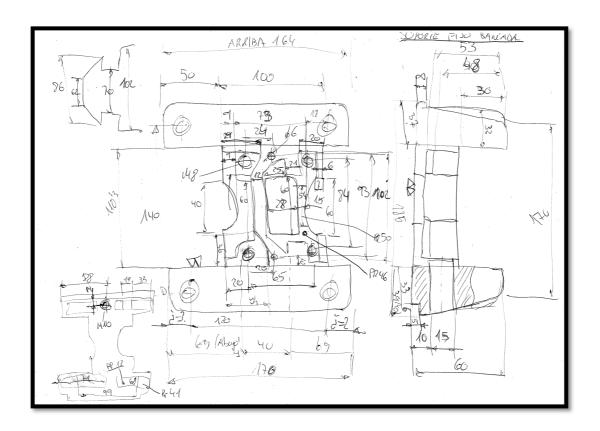
Croquis 11 <u>Pieza unión a encoder lineal</u>

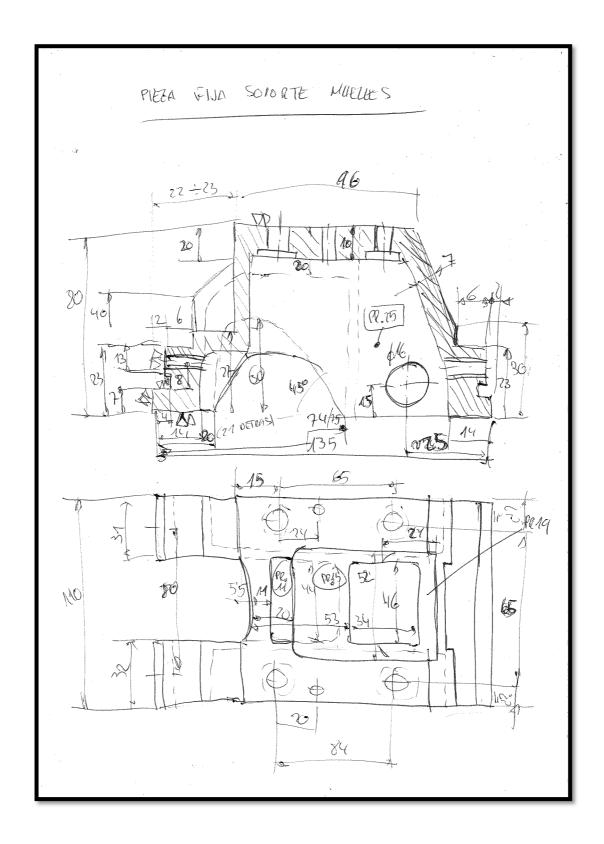


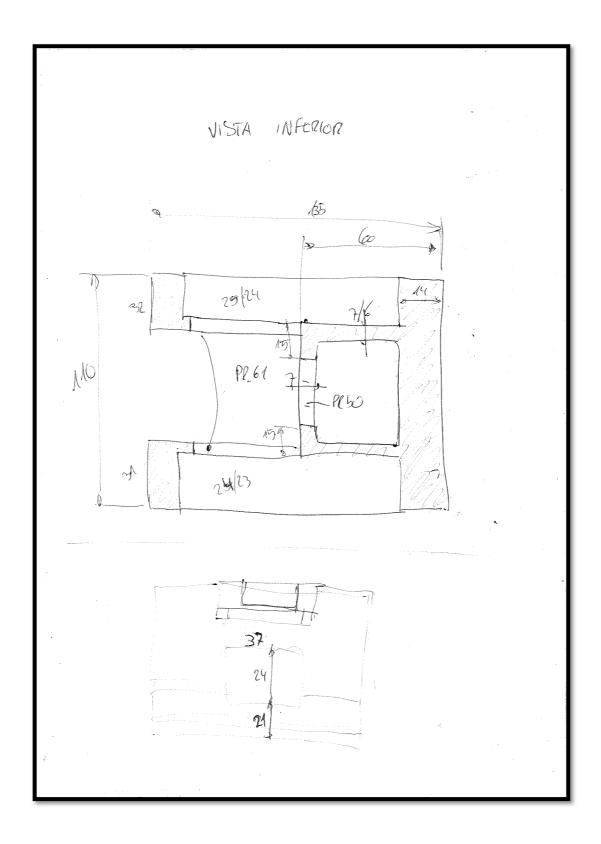
Croquis 12 <u>Maneta y leva bloqueo columna</u>



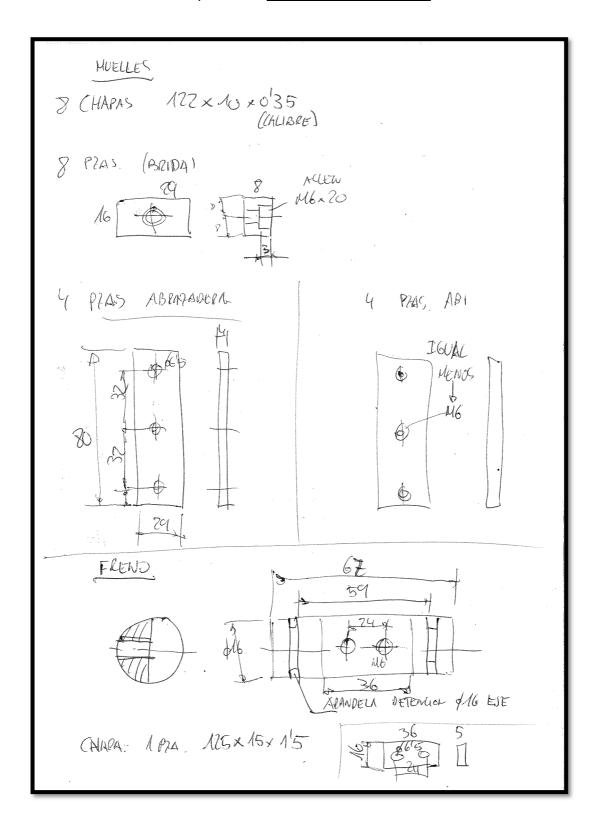
Croquis 13 Base columna unión a bancada



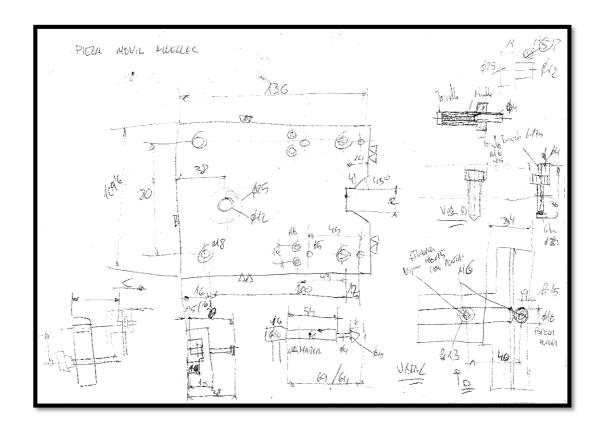


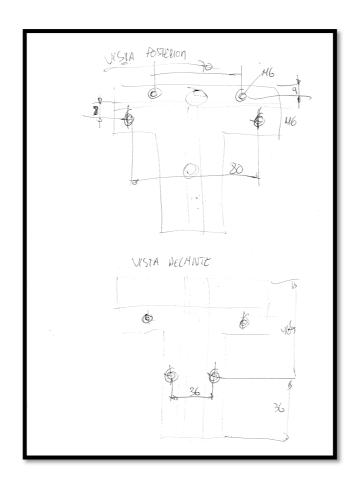


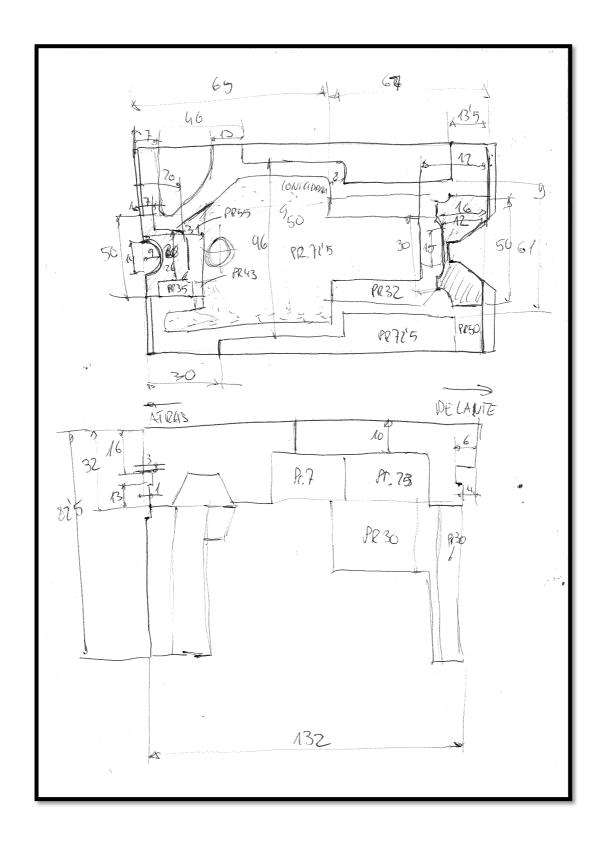
Croquis 14 Sistema elástico columna



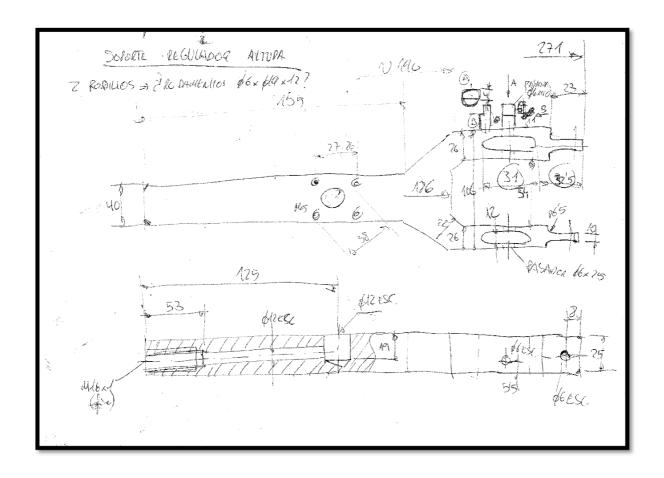
Croquis 15 <u>Base sistema elástico</u>

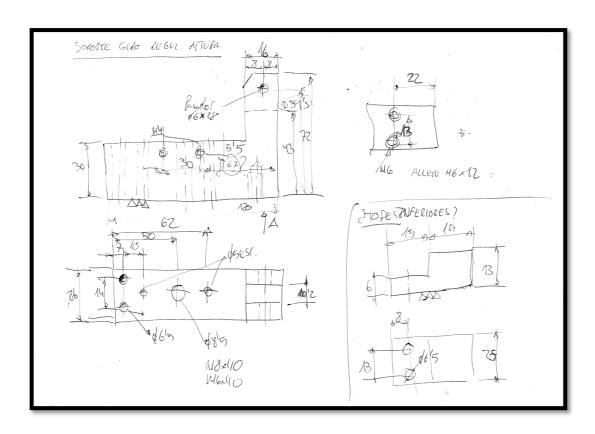




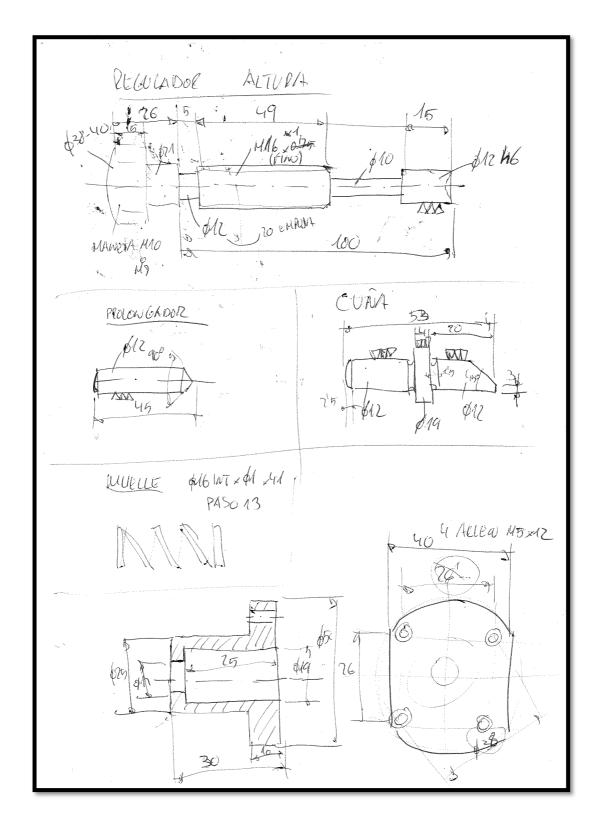


Croquis 16 Soporte regulación altura corona

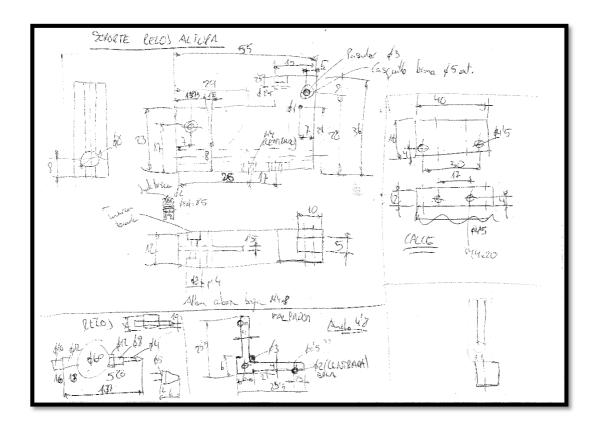




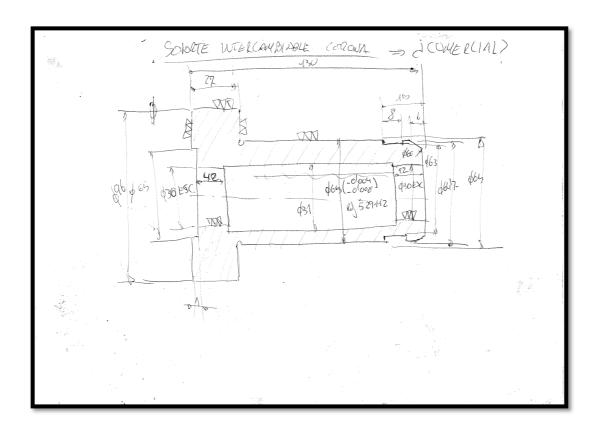
Croquis 17 <u>Actuador regulación altura corona</u>



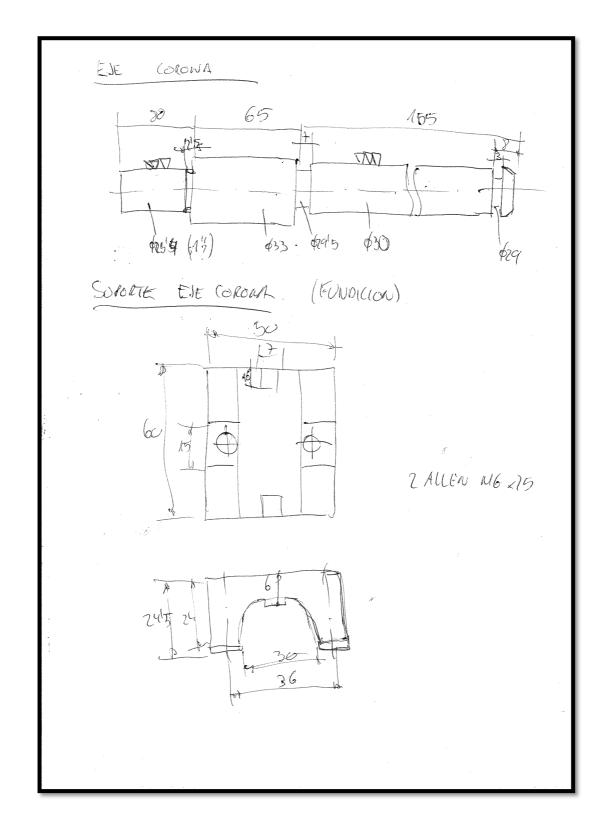
Croquis 18 Control altura corona



Croquis 19 <u>Utillaje corona</u>



Croquis 20 Eje soporte utillaje corona



# **ANEXO II: Características Técnicas Componentes Seleccionados**

En este anexo se incluye toda la documentación técnica y catálogos de los nuevos componentes de medida seleccionados y sus posibles alternativas descritos en el apartado 2.4.2 de la memoria.

## Los documentos son:

DOC. 1	ACCIONAMIENTO SINFÍN FAULHABER 3257G	. A-33
DOC. 2	ENCODER LINEAL CARRO PORTA-SINFÍN HEIDENHAIN LF481C	. A-43
DOC. 3	ALTERNATIVA ENCODER LINEAL HEIDENHAIN LF183	. A-56
DOC. 4	ALTERNATIVAS ENCODER LINEAL RENISHAW	. A-58
DOC. 5	PALPADOR LINEAL HEIDENHAIN-SPECTO ST1288	A-62
DOC. 6	ALTERNATIVA PALPADOR LINEAL HEIDENHAI-METRO MT1281	. A-71
DOC. 7	ALTERNATIVA PALPADOR MARPOSS HBT 3441557005	. A-72
DOC. 8	RELOJ COMPARADOR ALTURA CORONA TESA DIGICO 305M	. A-81

## Doc. 1 Accionamiento sinfín FAULHABER 3257G





#### DC-Micromotors

Technical Information

#### **General information**

The lifetime, depending on the application type, may exceed the 10 000 hours. Higher speeds cause accelerated mechanical wear, resulting in reduced lifetime. Also excessively high current and temperature shortens the lifetime. On the average, lifetime of up to 1 000 hours for metal brushes, and more than 3 000 hours for graphite brushes can be expected when the motors are operated within recommended values indicated on the data sheet. These values do not influence each other. It is advisable that the current under load in continuous operation should not be higher than one third of the stall current. In motors with graphite brushes the relationship between stall current and current under load depends on the delivered power and frame size. The motors should not be operated at the stall torque Mr. otherwise after a short period of time, the commutation or the windings could be

The motor develops its maximum power P2 max, at exactly half the stall torque MH which also corresponds to half the speed. For reasons of life performance, this working point should only be selected for intermittent periods. For exceptional long life performance, brushless DC-Motors are available.

#### Unspecified tolerances:

Tolerances in accordance with ISO 2768 medium.

≤ 6 -±0,1 mm < 30 - ± 0,2 mm < 120 - ± 0,3 mm

Motors with tighter tolerances and tolerances of values not specified are given on request.

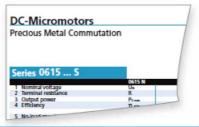
#### Bearing options:

- Standard:	Unless otherwise stated, vacuum Impregnated sintered bearings are used
- Optional:	Shielded ball bearings

#### Motor shaft:

All dimensions with shaft pushed against motor.

The listed motor types represent standardised executions. However, a variety of further coil possibilities are available.



#### Notes on technical data

All values at 22 °C. All values at nominal voltage, motor only, without load

#### Nominal voltage U<sub>N</sub> [Volt]

The nominal voltage at which all other characteristics indicated are measured.

#### Terminal resistance R [Ω] ±12%

The resistance measured across the motor terminals. The value is directly affected by the coil temperature (temperature coefficient:  $\alpha_{22} = 0,004 \text{ K}^{-1}$ ).

Output power P2 mec. [W]
The maximum obtainable mechanical power achieved at the nominal voltage.

$$P_{2 \text{ max.}} = \frac{R}{4} \cdot \left(\frac{U_N}{R} - I_0\right)^2$$

## Efficiency η<sub>max</sub>.[%]

The max. ratio between the absorbed electrical power and the obtained mechanical power of the motor. It does not always correspond to the optimum working point of the motor

$$\eta_{max.} = \left(1 - \sqrt{\frac{I_0 \cdot R}{U_N}}\right)^2 \cdot 100$$

## No-load speed no [rpm] ±12%

Describes the maximum speed under no-load conditions at steady state and 22 °C ambient temperature. If not otherwise defined the tolerance for the no-load speed is assumed to be ±12%.

#### No-load current I. [A] ±50%

Describes the current consumption of the motor without load at an ambient temperature of 22°C after reaching a steady state condition. The tolerance is given at +/-50%.



#### **DC-Micromotors**

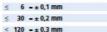
Technical Information

The lifetime, depending on the application type, may exceed the 10 000 hours. Higher speeds cause accelerated mechanical wear, resulting in reduced lifetime. Also excessively high current and temperature shortens the lifetime. On the average, lifetime of up to 1 000 hours for metal brushes, and more than 3 000 hours for graphite brushes can be expected when the motors are operated within recommended values indicated on the data sheet. These values do not influence each other. It is advisable that the current under load in continuous operation should not be higher than one third of the stall current. In motors with graphite brushes the relationship between stall current and current under load depends on the delivered power and frame size. The motors should not be operated at the stall torque MH, otherwise after a short period of time, the commutation or the windings could be

The motor develops its maximum power P2 max at exactly half the stall torque Mn which also corresponds to half the speed. For reasons of life performance, this working point should only be selected for intermittent periods. For exceptional long life performance, brushless DC-Motors are available.

#### Unspecified tolerances:

Tolerances in accordance with ISO 2768 medium.



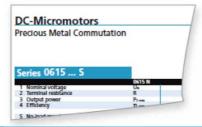
Motors with tighter tolerances and tolerances of values not specified are given on request.

bearing optio	nsi	
- Standard:	Unless otherwise stated, vacuum impregnated sintered bearings are used	
- Optional:	Shielded hall bearings	

#### Motor shaft:

All dimensions with shaft pushed against motor.

The listed motor types represent standardised executions. However, a variety of further coil possibilities are available.



#### Notes on technical data

All values at 22 °C. All values at nominal voltage, motor only, without load.

#### Nominal voltage U<sub>N</sub> [Volt]

The nominal voltage at which all other characteristics indicated are measured.

#### Terminal resistance R [Ω] ±12%

The resistance measured across the motor terminals. The value is directly affected by the coil temperature (temperature coefficient: azz = 0,004 K-1).

Output power P2 mes. [W] The maximum obtainable mechanical power achieved at the nominal voltage.

$$P_{2 \text{ max.}} = \frac{R}{4} \cdot \left(\frac{U_N}{R} - I_o\right)^2$$

### Efficiency η<sub>mer.</sub>[%]

The max. ratio between the absorbed electrical power and the obtained mechanical power of the motor. It does not always correspond to the optimum working point of the motor.

$$\eta_{max.} = \left(1 - \sqrt{\frac{I_0 \cdot R}{U_N}}\right)^2 \cdot 100$$

#### No-load speed no [rpm] ±12%

Describes the maximum speed under no-load conditions at steady state and 22 °C ambient temperature. If not otherwise defined the tolerance for the no-load speed is assumed to be ±12%.

$$n_o = (U_N - I_o \cdot R) \cdot k_n$$

#### No-load current lo [A] ±50%

Describes the current consumption of the motor without load at an ambient temperature of 22°C after reaching a steady state condition. The tolerance is given at +/-50%.



The no-load current is speed and temperature dependent. Changes in ambient temperature or cooling conditions will influence the value. In addition, modifications to the shaft, bearing, lubrication, and commutation system or combinations with other components such as gearheads or encoders will all result in a change to the no-load current of the motor.

#### Stall torque Ma [mNm]

The torque developed by the motor at zero speed and nominal voltage. This value is greatly influenced by temperature.

$$M_H = k_M \cdot \left( \frac{U_N}{R} - l_o \right)$$

#### Friction torque MR [mNm]

Torque losses caused by the friction of brushes, bearings and commutators. This value is influenced by temperature.

#### Speed constant kn [rpm/V]

The speed variation per Volt applied to the motor terminals at constant load.

$$k_n = \frac{n_s}{U_N - I_s \cdot R} = \frac{1000}{k_s}$$

#### Back-EMF constant ks [mV/rpm]

The constant corresponding to the relationship between the induced voltage in the rotor at the speed of rotation.

$$k_t = \frac{2\pi \cdot k_M}{60}$$

#### Torque constant km [mNm/A]

The constant corresponding to the relationship between the torque developed by the motor and the current drawn.

#### Current constant & [A/mNm]

The constant between the current in the motor and the torque developed.

$$k_i = \frac{1}{k_{ij}}$$

#### Slope of n-M curve \( \Delta n / \Delta M \) [rpm/mNm]

The ratio of the speed variation to the torque variation. The smaller the value, the more powerful the motor.

$$\frac{\Delta n}{\Delta M} = \frac{30000}{\pi} \cdot \frac{R}{k_{H}^2}$$

## Rotor inductance L [µH]

The inductance measured on the motor terminals at 1 kHz.

#### Mechanical time constant Tm [ms]

The time required for the motor to reach a speed of 63% of its final no-load speed, from standstill.



### Rotor inertia J [gcm²]

Rotor's mass dynamic inertia moment.

#### Angular acceleration α max. [-103 rad/s2]

The acceleration obtained from standstill under no-loadconditions and at nominal voltage.

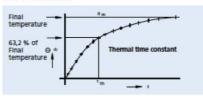
#### Thermal resistance Rths/Rthz [K/W]

Reh corresponds to the value between the rotor and housing. Reh corresponds to the value between the housing and the ambient air.

 $R_{\rm th2}$  can be reduced by enabling exchange of heat between the motor and the ambient air (for example using a heat sink or forced air cooling).

#### Thermal time constant Tw1/Tw2 [5]

The thermal time constant specifies the time needed for the rotor and housing to reach a temperature equal to 63% of final value.



#### Operating temperature range [°C]

Indicates the min. and max. motor operating temperature, as well as the maximum permitted rotor temperature.

#### Shaft bearings

The bearings used for the DC-Micromotors.

#### Shaft load max. [N]

The output shaft load at a specified shaft diameter for the primary output shaft. For motors with ball bearings the load and lifetime are in accordance with the values given by the bearing manufacturers. This value does not apply to second, or rear shaft ends.

## Shaft play [mm]

The shaft play on the bearings, measured at the bearing

#### Housing material

The housing material and the surface protection.

#### Weight [g]

The average weight of the basic motor type.



## **DC-Micromotors**

Technical Information

## Direction of rotation

The direction of rotation is viewed from the front face. Positive voltage to the + terminal gives clockwise rotation of the motor shaft. All motors are designed for clockwise (CW) and counterclockwise (CCW) operation; the direction of rotation is reversible.

### Recommended values

The maximum recommended values for continuous operation to obtain optimum life performance are listed below. The values are independent of each other. The values will be reduced with thermal insulation and elevated temperature but can be increased with forced cooling.

## Speed nomm. [rpm]

The maximum recommended operating speed.

## Torque Momax. [mNm]

The maximum recommended torque rating.

## Current Is max. [A]

The maximum allowable current, based on the thermal limits of the max. permissible standard rotor temperature at 22 °C ambient.

## How to select a DC-Micromotor

This section reviews a step-by-step procedure on how to select a DC-Micromotor. The procedure allows calculation of the parameters in order to produce a graph of the characteristics and per-mitting the definition of the motor's behaviour. To simplify the calculation, in this example continuous operation and optimum life performance are assumed and the influence of temperature and tolerances has been omitted.

## Application data:

The basic data required for any given application are:

Required torque	M	[mNm]
Required speed	n	[rpm]
Duty cycle	0	[%]
Available supply voltage, max.	U	IV DCI
Available current source, max.	1	[A]
Avallable space, max.	diameter/length	[mm]
Shaft load	radial/axial	[N]

The assumed application data for the selected example are:

Output torque

M = 3 mNm
Speed n = 5 500 rpm

Duty cycle	0	- 100	%
Supply voltage	U	- 20	V DC
Current source, max.	1	- 0,5	A
Space max.	dlameter	- 25	mm
	length	- 50	mm
Shaft load	radial	- 1,0	N
	axial	-0,2	N

### Preselection

The first step is to calculate the power the motor is expected to deliver:

$$P_2 = M \cdot n \frac{\pi}{30 \cdot 1000}$$
 [W]  
 $P_2 = 3.5500 \frac{\pi}{30.1000} = 1,73$  W

A motor is then selected from the catalogue which will give at least 1,5 to 2 times the output power  $[P_{2 \text{ max}}]$  than the one obtained by calculation, and where the nominal voltage is equal to or higher than the one required in the application data.

The physical dimensions (diameter and length) of the motor selected from the data sheets should not exceed the available space in the application.

The motor selected from the catalogue for this particular application, is series 2233 T 024 S with the following characteristics:

Nominal voltage		Uw	- 24	VDC
Output power, max.		P2 max.	- 2,47	W
Frame size:	dlameter	Ø	- 22	mm
	length	L	- 33	mm
Shaft load, max.:		radial	- 1,2	N
		axial	- 0,2	N
No-load current		l <sub>p</sub>	- 0,005	A
No-load speed		n <sub>o</sub>	- 8 800	rpm
Stall torque		Мн	- 10.70	mNm

## Caution:

Should the available supply voltage be lower than the nominal voltage of the selected DC-Micromotor, it will be necessary to calculate [P2 mw.] with the following equation:

$$P_{2max} = \frac{R}{4} \cdot \left(\frac{U_N}{R} - I_n\right)^2$$
 [W]  
 $P_{2max} (20 \text{ V}) = \frac{57}{4} \cdot \left(\frac{20}{57} - 0,005\right)^2 = 1,70 \text{ W}$ 



### Optimizing the preselection

To optimize the motor's operation and life performance, the required speed [n] has to be higher than half the no-load speed  $[n_o]$  at nominal voltage, and the load torque [M] has to be less than half the stall torque [Mn].

$$n \ge \frac{n_0}{2}$$
  $M \le \frac{M_H}{2}$ 

From the data sheet for the DC-Micromotor, 2233 T 024 S the parameters meet the above requirements.

$$n (5 500 \text{ rpm}) \ge \frac{n_s}{2}$$
 is greater than  $\frac{8 800}{2} = 4 400 \text{ rpm}$   
 $M (3 \text{ mNm}) \le \frac{M_{H}}{2}$  is less  $\frac{10,70}{2} = 5,35$  mNm

This DC-Micromotor will be a good first choice to test in this application. Should the required speed [n] be less than half the no-load speed  $[n_o]$ , and the load torque [M] be less than half the stall torque  $[M_n]$ , try the next voltage motor up.

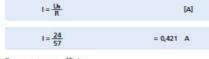
Should the required torque [M] be compliant but the required speed [n] be less than half the no-load speed [n<sub>o</sub>], try a lower supply voltage or another smaller frame size motor.

Should the required speed be well below half the no-load speed and or the load torque [M] be more than half the stall torque [MH], a gearhead or a larger frame size motor has to be selected.

## Performance characteristics at nominal voltage (24 V DC)

A graphic presentation of the motor's characteristics can be obtained by calculating the stall current [I] and the torque [M] at its point of max. efficiency [M<sub>spr.</sub>]. All other parameters are taken directly from the data sheet of the selected motor.

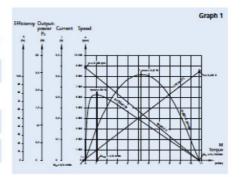
Stall current



Torque at max. efficiency

$$M_{opt} = \sqrt{M_{tr} \cdot M_{tr}}$$
 [mNm] 
$$M_{opt} = \sqrt{10,70 \cdot 0,13}$$
 = 1,18 mNm

It is now possible to make a graphic presentation and draw the motor diagram (see graph 1).



### Calculation of the main parameters

In this application the available supply voltage is lower than the nominal voltage of the selected motor. The calculation under load therefore is made at 20 V DC.

### No-load speed n₀ at 20 V DC

MH = 25,70 (0,351 - 0,005)

$n_o = \frac{U - (I_o \cdot R)}{K_g} \cdot 1000$			[rpm]
inserting the values			
Supply voltage	U	- 20	V DC
Terminal resistance	R	- 57	Ω.
No-load current	lo	- 0,005	A
Back-EMF constant	Kr	- 2,690	mWrpm

$n_o = \frac{20 - (0,005 \cdot 57)}{2,690} \cdot 1000$	
Stall current la	= 7 315 rpm
$I_{ii} = \frac{U}{R}$	
$I_{H} = \frac{20}{57}$	[A]

57		
Stall torque Mn		= 0,351 A
$M_{ii} = k_{in}(I_{ii} - I_{ii})$		
inserting the value		[mater]
Torque constant	Км	- 25,70 (MNH)A

- 8,91 mNm



## **DC-Micromotors**

**Technical Information** 

Output power, max. P2 max.

$$P_{2 \text{ max}} = \frac{R}{4} \cdot \left(\frac{U_N}{R} - I_0\right)^2$$
 [W]

$$P_{2 \text{ max}}(20 \text{ V}) = \frac{57}{4} \cdot \left(\frac{20}{57} - 0,005\right)^2 = 1,70 \text{ W}$$

Efficiency, max. η<sub>mer.</sub>

$$\eta_{\text{max.}} = \left(1 - \sqrt{\frac{I_0}{I_H}}\right)^2 \cdot 100$$
 [%]

$$\eta_{\text{max}} = \left(1 - \sqrt{\frac{0,005}{0,351}}\right)^2 \cdot 100 = 77,6 96$$

At the point of max. efficiency, the torque delivered is:

$M_{opt.} = \sqrt{M_H \cdot M_R}$				[mNm]
inserting the values				
Friction torque	Ma	-	0,13	mNm
and Stall torque at 20 V DC	Мн	-	8,91	mNm
M \( \overline{9.91 \cdot 0.13} \)			- 1.08	mNm

Calculation of the operating point at 20 V DC When the torque (M=3 mNm) at the working point is taken into consideration I, n,  $P_2$  and  $\eta$  can be calculated:

Current at the operating point

$$I = \frac{M + M_{IL}}{k_{id}}$$
 [A]  
 $I = \frac{3 + 0.13}{25.70}$  = 0.122 A

Speed at the operating point

$$n = \frac{U - R \cdot l}{k_L} \cdot 1000$$
 [rpm]  
$$n = \frac{20 - 57 \cdot 0.122}{2.690} \cdot 1000$$
 = 4.841 rpm

Output power at the operating point

$$P_2 = M \cdot n \cdot \frac{\pi}{30 \cdot 1000}$$
 [W]  
 $P_2 = 3 \cdot 4841 \cdot \frac{\pi}{30 \cdot 1000} = 1,52$  W

Efficiency at the operating point



In this example the calculated speed at the working point is different to the required speed, therefore the supply voltage has to be changed and the calculation repeated.

## Supply voltage at the operating point

The exact supply voltage at the operating point can now be obtained with the following equation:

In this calculated example, the parameters at the operating point are summarized as follows:

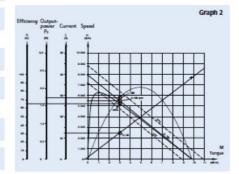
Supply voltage	U	- 21,78	V DC
Speed	n	- 5 500	rpm
Output torque	Mn	- 3	mNm
Current	I	- 0,12	A
Output power	P <sub>2</sub>	- 1,72	W
Efficiency	η	- 66	%

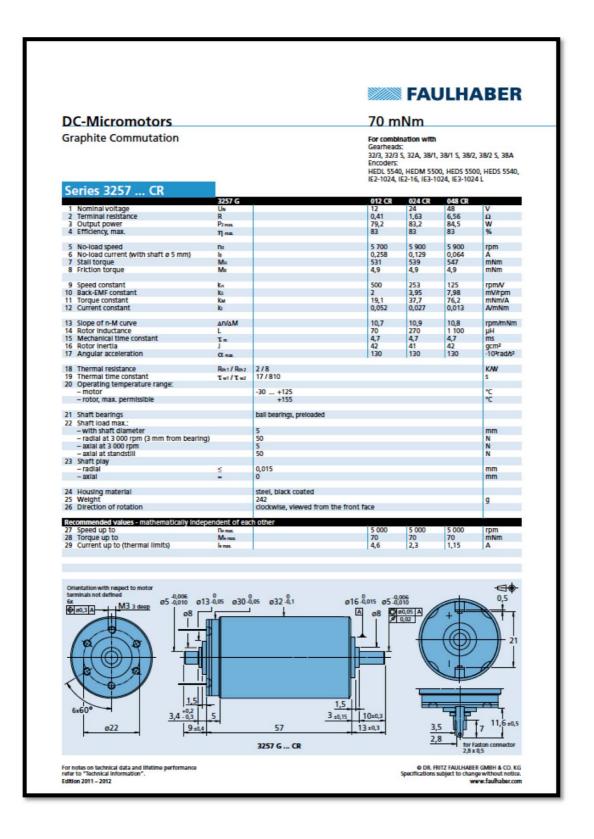
## Motor characteristic curves

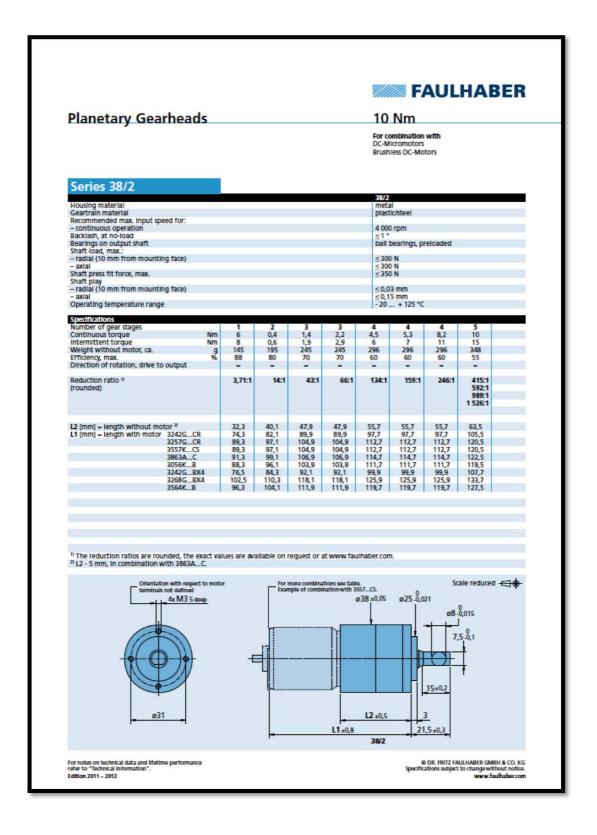
For a specific torque, the various parameters can be read on graph 2.

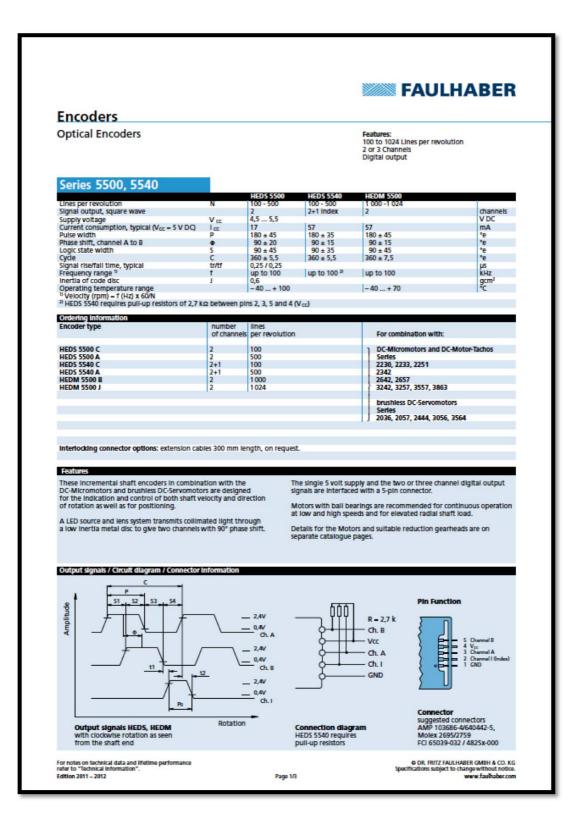
To simplify the calculation, the influence of temperature and tolerances has deliberately been omitted.

In certain cases the influence of temperature should, however, be taken into consideration.

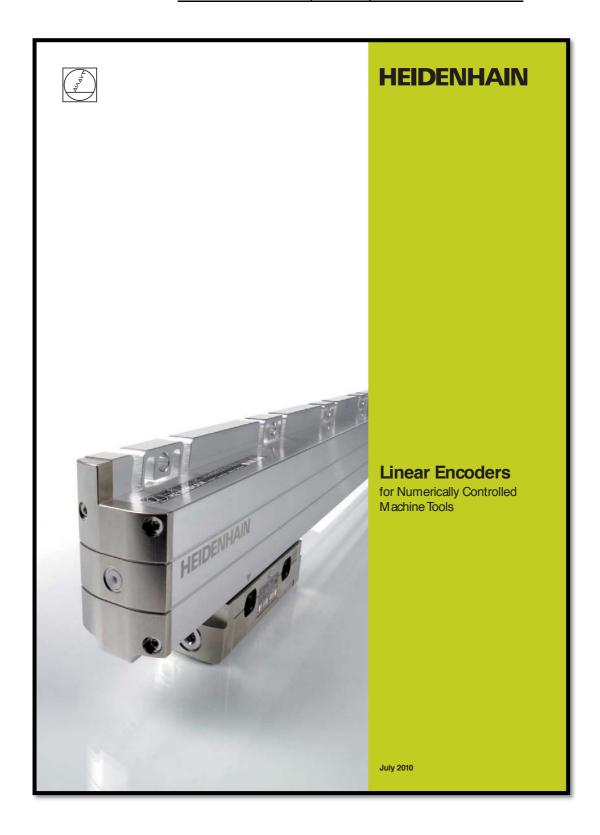








# Doc. 2 <u>Encoder lineal carro porta-sinfín HEIDENHAIN LF481C</u>



# Measuring Principles Measuring Standard

HEIDENHAIN encoders with optical scanning incorporate measuring standards of periodic structures known as graduations

or periodic structures wawmas graduations. These graduations are applied to a carrier substrate of glass or steel. The scale substrate for large measuring lengths is a steel tape.

These precision graduations are manufactured in various photolithographic processes. Graduations can be fabricated from:

- extremely hard chromium lines on glass,matte-etched lines on gold-plated steel
- matte-etched lines on gold-plated steel tape, or
- three-dimensional grid structures on glass or steel substrates.

The photolithographic manufacturing processes developed by HEIDENHAIN produce grating periods of typically 40  $\mu\rm m$  to 4  $\mu\rm m$ .

Along with these very fine grating periods, these processes permit a high definition and homogeneity of the line edges. Together with the photoelectric scanning method, this high edge definition is a precondition for the high quality of the output signals.

The master graduations are manufactured by HEIDENHAIN on custom-built high-precision ruling machines.

# Absolute Measuring Method

With the absolute measuring method, the position value is available from the encoder immediately upon switch-on and can be called at any time by the subsequent electronics. There is no need to move the axes to find the reference position. The absolute position information is read from the scale graduation, which is formed from a serial absolute code structure. A separate incremental track is interpolated for the position value and at the same time is used to generate an optional incremental signal.



Graduation of an absolute linear encoder



Schematic representation of an absolute code structure with an additional incremental track (LC 483 as example)

# Incremental Measuring Method

With the incremental measuring method, the graduation consists of a periodic grating structure. The position information is obtained by counting the individual increments (measuring steps) from some point of origin. Since an absolute reference is required to ascertain positions, the scales or scale tapes are provided with an additional track that bears a reference mark. The absolute position on the scale, established by the reference mark, is gated with exactly one signal period. The reference mark must therefore be scanned to establish an absolute reference or to find the last selected datum.

In some cases this may necessitate machine movement over large lengths of the measuring range. To speed and simplify such "reference runs," many encoders feature distance-coded reference marks—multiple reference marks that are individually spaced according to a mathematical algorithm. The subsequent electronics find the absolute reference after traversing two successive reference marks—only a few millimeters traverse (see table).

Encoders with distance-coded reference marks are identified with a "C" behind the model designation (e.g. LS 487C).

With distance-coded reference marks, the absolute reference is calculated by counting the signal periods between two reference marks and using the following formula:



 $P_1 = (abs B-sgn B-1) \times \frac{N}{2} + (sgn B-sgn D) \times \frac{abs M_{RR}}{2}$ 

where

 $B = 2 \times M_{RR}-N$ 

and:

P<sub>1</sub> = Position of the first traversed reference mark in signal periods

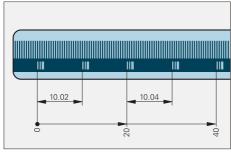
abs = Absolute value

sgn = Sign function (" +1" or " -1")

M<sub>RR</sub> = Number of signal periods between the traversed reference marks

- Nominal increment between two fixed reference marks in signal periods (see table below)
- Direction of traverse (+1 or -1).
   Traverse of scanning unit to the right (when properly installed) equals +1.

Graduations of incremental linear encoders



Schematic representation of an incremental graduation with
distance-coded reference marks (LS as example)

	Signal period	Nominal increment N in signal periods	Maximum traverse
LF	4 μm	5000	20 mm
LS	20 μm	1000	20 mm
LB	40 μm	2000	80 mm

Marcos Pueo Arteta Trabajo Fin de Master

# Photoelectric Scanning

Most HEIDENHAIN encoders operate using the principle of photoelectric scanning. The photoelectric scanning of a measuring standard is contact-free, and therefore without wear. This method detects even very fine lines, no more than a few microns wide, and generates output signals with very small signal periods.

The finer the grating period of a measuring standard is, the greater the effect of diffraction on photoelectric scanning. HEIDENHAIN uses two scanning principles with linear encoders:

- The imaging scanning principle for grating periods from 20 μm and 40 μm
   The interferential scanning principle for very fine graduations with grating periods of 8  $\mu$ m and smaller.

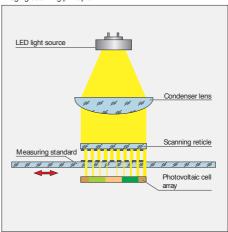
Imaging scanning principle
To put it simply, the imaging scanning principle functions by means of projected-light signal generation: two scale gratings with equal or similar grating periods are moved relative to each other—the scale and the scanning reticle. The carrier material of the scanning reticle is transparent, whereas the graduation on the measuring standard may be applied to a transparent or reflective surface.

When parallel light passes through a grating, light and dark surfaces are projected at a certain distance, where there is an index grating. When the two gratings move relative to each other, the incident light is modulated. If the gaps in the gratings are aligned, light passes through. If the lines of one grating coincide with the gaps of the other, no light passes through. An array of photovoltaic cells converts these variations in light intensity into electrical signals. The specially structured grating of the scanning reticle filters the light current to generate nearly sinusoidal output signals.

The smaller the period of the grating structure is, the closer and more tightly toleranced the gap must be between the scanning reticle and scale.

The LC, LS and LB linear encoders operate according to the imaging scanning principle.

## Imaging scanning principle



### Interferential scanning principle

The interferential scanning principle exploits the diffraction and interference of light on a fine graduation to produce signals used to measure displacement.

A step grating is used as the measuring standard: reflective lines  $0.2\,\mu\mathrm{m}$  high are applied to a flat, reflective surface. In front of that is the scanning reticle—a transparent phase grating with the same grating period as the scale.

When a light wave passes through the scanning reticle, it is diffracted into three partial waves of the orders –1, 0, and +1, with approximately equal luminous intensity. The waves are diffracted by the scale such that most of the luminous intensity is found in the reflected diffraction orders +1 and –1. These partial waves meet again at the phase grating of the scanning reticle where they are diffracted again and interfere. This produces essentially three waves that leave the scanning reticle at different angles. Photovoltaic cells convert this alternating light intensity into electrical signals.

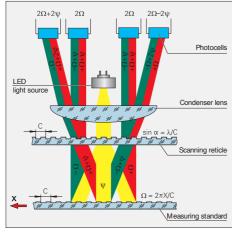
A relative motion of the scanning reticle to the scale causes the diffracted wave fronts to undergo a phase shift: when the grating moves by one period, the wave front of the first order is displaced by one wavelength in the positive direction, and the wavelength in of diffraction order—I is displaced by one wavelength in the negative direction. Since the two waves interfere with each other when exiting the grating, the waves are shifted relative to each other by two wavelengths. This results in two signal periods from the relative motion of just one grating period.

Interferential encoders function with grating periods of, for example, 8  $\mu$ m, 4  $\mu$ m and finer. Their scanning signals are largely free of harmonics and can be highly interpolated. These encoders are therefore especially suited for high resolution and high accuracy.

Sealed linear encoders that operate according to the interferential scanning principle are given the designation LF.

Interferential scanning principle (optics schematics)

- C Grating period
- Ψ Phase shift of the light wave when passing through the scanning reticle
- $\Omega\,$  Phase shift of the light wave due to motion X of the scale



# **Measuring Accuracy**

The accuracy of linear measurement is mainly determined by:

- The quality of the graduation
  The quality of the scanning process
- The quality of the signal processing electronics
- The error from the scanning unit guideway to the scale

A distinction is made between position errors over relatively large paths of traverse—for example the entire measuring length-and those within one signal period.

## Position error over the measuring range

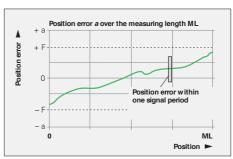
The accuracy of sealed linear encoders is specified in grades, which are defined as follows:

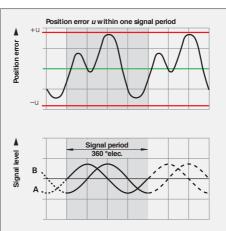
The extreme values  $\pm$  F of the measuring curves over any max. one-meter section of the measuring length lie within the accuracy grade  $\pm$  a. They are ascertained during the final inspection, and are indicated on the calibration chart.

With sealed linear encoders, these values apply to the complete encoder system including the scanning unit. It is then referred to as the system accuracy.

Position error within one signal period The position error within one signal period is determined by the signal period of the encoder, as well as the quality of the graduation and the scanning thereof. At any measuring position, it does not exceed  $\pm$  2% of the signal period, and for the LC and LS linear encoders it is typically  $\pm$  1%. The smaller the signal period, the smaller the position error within one signal period.

	Signal period of scanning signals	Max. position error <i>u</i> within one signal period
LF	4 μm	Approx. 0.08 μm
LC	20 μm	Approx. 0.2 µm
LS	20 μm	Approx. 0.2 µm
LB	40 μm	Approx. 0.8 µm





All HEIDENHAIN linear encoders are inspected before shipping for positioning accuracy and proper function. **HEIDENHAIN** The position errors are measured by traversing in both directions, and the averaged curve is shown in the calibration The Quality Inspection Certificate confirms the specified system accuracy of each encoder. The calibration standards LC 483 ID 557649-09 SN 19765168 Qualitätsprüf-Zertifikat Quality Inspection Certificate ensure the traceability—as required by ISO 9001—to recognized national or international standards. Positionsabweichung F (µm) Position error F (µm) For the LC, LF and LS series listed in this brochure, a calibration chart documents the additional **position error** over the measuring length. The measurement parameters and uncertainty of the measuring machine are also stated. **Temperature range**The linear encoders are inspected at a reference temperature of 20 °C. The system accuracy given in the calibration chart applies at this temperature. The operating temperature range indicates the ambient temperature limits between which the linear encoders will between which the linear encoders will function properly. The **storage temperature** range of –20 °C to 70 °C applies for the unit in its packaging. Starting from a measuring length of 3240 mm, the permissible storage temperature range for encoders of the LC 183/LC 193 series is restricted to –10 °C to +50 °C. 14.02.2007 Engoer Melmol Professionated by M. Kingson Example 13

# Mechanical Design Types and Mounting Guidelines

## Linear Encoders with Small Cross Section

The LC, LF and LS slimline linear encoders should be fastened to a machined surface over their entire length, especially for highly-dynamic requirements. Larger measuring lengths and higher vibration loads are made possible by using mounting spars or clamping elements (only for LC 4x3).

The encoder is mounted so that the sealing lips are directed downward or away from splashing water (also see *General Mechanical Information*).

## Thermal behavior

Because they are rigidly fastened using two M8 screws, the linear encoders largely adapt themselves to the mounting surface. When fastened over the mounting spar, the encoder is fixed at its midpoint to the mounting surface. The flexible fastening elements ensure reproducible thermal behavior.

The LF 481 with its graduation carrier of steel has the same coefficient of thermal expansion as a mounting surface of gray cast iron or steel.

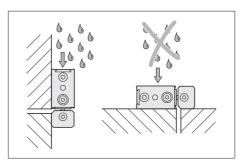
### Mounting

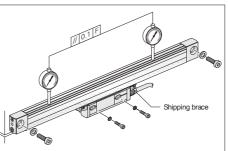
It is surprisingly simple to mount the sealed linear encoders from HEIDENHAIN: You need only align the scale unit at several points along the machine guideway. Stop surfaces or stop pins can also be used for this. The shipping brace already sets the proper gap between the scale unit and the scanning unit, as well as the lateral tolerance. If the shipping brace needs to be removed before mounting due to a lack of space, then the mounting gauge is used to set the gap between the scale unit and the scanning unit easily and exactly. You must also ensure that the lateral tolerances are maintained.

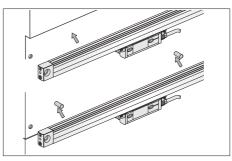
## Accessories

Mounting and test gauges for slimline linear encoders

The mounting gauge is used to set the gap between the scale unit and the scanning unit if the shipping brace needs to be removed before mounting. The test gauges are used to quickly and easily check the gap of the mounted linear encoder.







	x	Color	ID
Mounting gauge	1.0 mm	Gray	528753-01
Max. test gauge	1.3 mm	Red	528753-02
Min. test gauge	0.7 mm	Blue	528753-03



Along with the standard procedure of using two M8 screws to mount the scale unit on a plane surface, there are also other mounting possibilities:

Installation with mounting spar The use of a mounting spar can be of great benefit when mounting slimline linear encoders. They can be fastened as part of the machine assembly process. The encoder is then simply clamped on during final mounting. Easy exchange also facilitates servicing.

A mounting spar is recommended for highly-dynamic applications with ML greater than 640 mm. It is always necessary for measuring lengths starting from 1240 mm.

The universal mounting spar was developed specifically for the LC 4x3 and LS 4x7. It can be mounted very easily, since the components necessary for clamping are premounted. Linear encoders with normal head mounting blocks and-if compatibility considerations require them-linear encoders with short end blocks can be mounted. Other advantages:

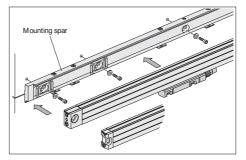
- · Mechanically compatible versions The universal mounting spar and the LC 4x3 and the LS 4x7 are compatible in their mating dimensions to the previous versions. Any combinations are possible, such as the LS 4x6 with the universal mounting spar, or the LC 4x3 with the previous mounting spar
- Freely selectable cable outlet
  The LC 4x3 and the LS 4x7 can be mounted with either side facing the universal mounting spar. This permits the cable exit to be located on the left or right—a very important feature if installation space is limited.

The universal mounting spar must be ordered separately, even for measuring lengths over 1240 mm.

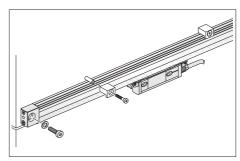
Accessory: Universal mounting spar ID 571 613-xx

Mounting with clamping elements The scale unit of the LC 4x3 is fastened at both ends. In addition, it can also be attached to the mounting surface by clamping elements. This way the fastening at the center of the measuring length (recommended for highly-dynamic applications with ML greater than 620 mm) is easy and reliable. This makes mounting without the mounting spar possible for measuring lengths greater than 1240 mm.

Clamping elements
With pin and M5x10 screw ID 556975-01 (10 units per package)







# Linear Encoders with Large Cross Section

The LB, LC, LF and LS full-size linear encoders are fastened over their entire length onto a machined surface. This gives them a **high vibration rating**. The inclined arrangement of the sealing lips permits universal mounting with vertical or horizontal scale housing with equally high protection rating.

### Thermal behavior

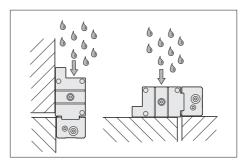
The thermal behavior of the LB, LC, LF and LS 100 linear encoders with large cross section has been optimized:

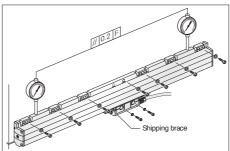
On the **LF** the steel scale is cemented to a steel carrier that is fastened directly to the machine element.

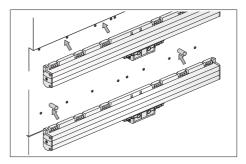
On the LB the steel scale tape is clamped directly onto the machine element. The LB therefore takes part in all thermal changes of the mounting surface.

LC and LS are fixed to the mounting surface at their midpoint. The flexible fastening elements permit reproducible thermal behavior.

**Mounting**It is surprisingly simple to mount the sealed linear encoders from HEIDENHAIN: You need only align the scale unit at several you need only aligh the scale unit at severa points along the machine guideway. Stop surfaces or stop pins can also be used for this. The shipping brace already sets the proper gap between the scale unit and the scanning unit. The lateral gap is to be set during mounting. If the shipping brace scale to be removed to the proper properties due. needs to be removed before mounting due to a lack of space, then the mounting gauge is used to set the gap between the scale unit and the scanning unit easily and exactly. You must also ensure that the lateral tolerances are maintained.







Mounting the multi-section LB 382
The LB 382 with measuring lengths over
3240 mm is mounted on the machine in
individual sections:

- Mount and align the individual housing sections
- sections
  Pull in the scale tape over the entire length and tension it
  Pull in the sealing lips
  Insert the scanning unit

Adjustment of the tensioning of the scale tape enables linear machine error compensation up to  $\pm$  100  $\mu$ m/m.

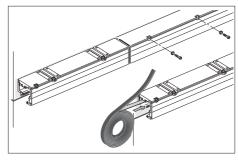
Accessory: Mounting aid for LC 1x3 and LS 1x7 ID 547793-01

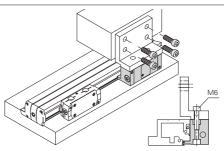
The mounting aid is locked onto the scale unit, simulating an optimally adjusted scanning unit. The customer's mating surface for the scanning unit can then be aligned to it. The mounting aid is then removed and the scanning unit is attached to the mounting bracket.

### Accessories:

Mounting and test gauges for full-size linear encoders

The **mounting gauge** is used to set the gap between the scale unit and the scanning unit if the shipping brace needs to be removed before mounting. The **test** gauges are used to quickly and easily check the gap of the mounted linear



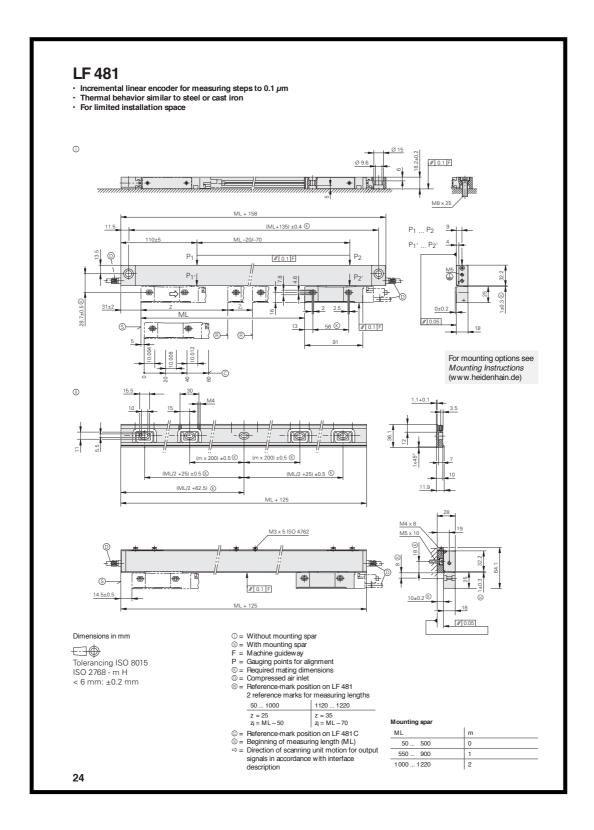


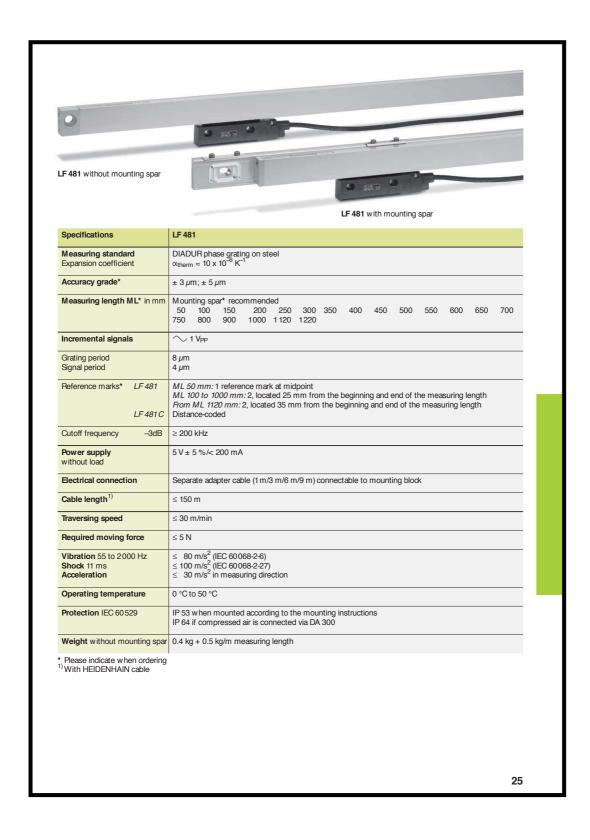
Example

LC, LS	x	Color	ID
Mounting gauge	1.5 mm	Gray	575832-01
Max. test gauge	1.8 mm	Red	575832-02
Min. test gauge	1.2 mm	Blue	575832-03

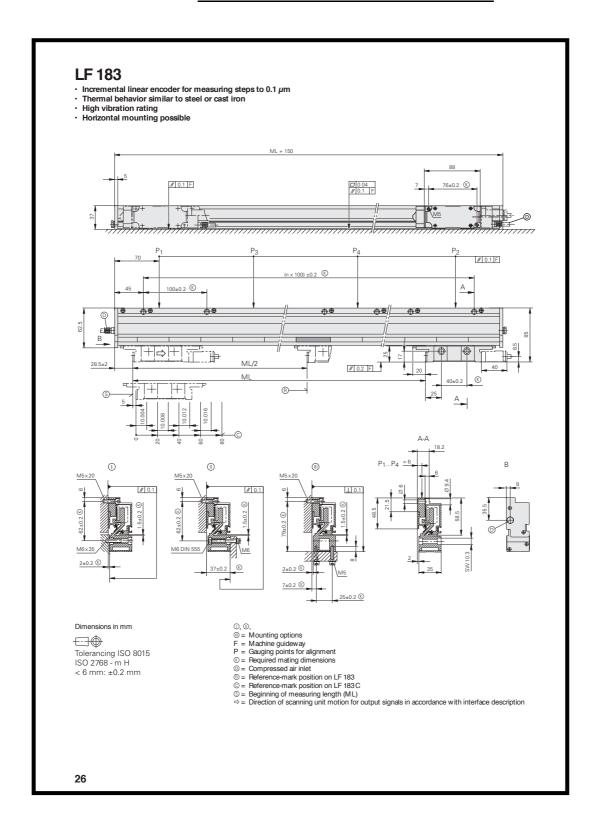
LB	x	Color	ID
Mounting gauge	1.0 mm	Gray	647933-01
Max. test gauge	1.3 mm	Red	647933-02
Min. test gauge	0.7 mm	Blue	647933-03







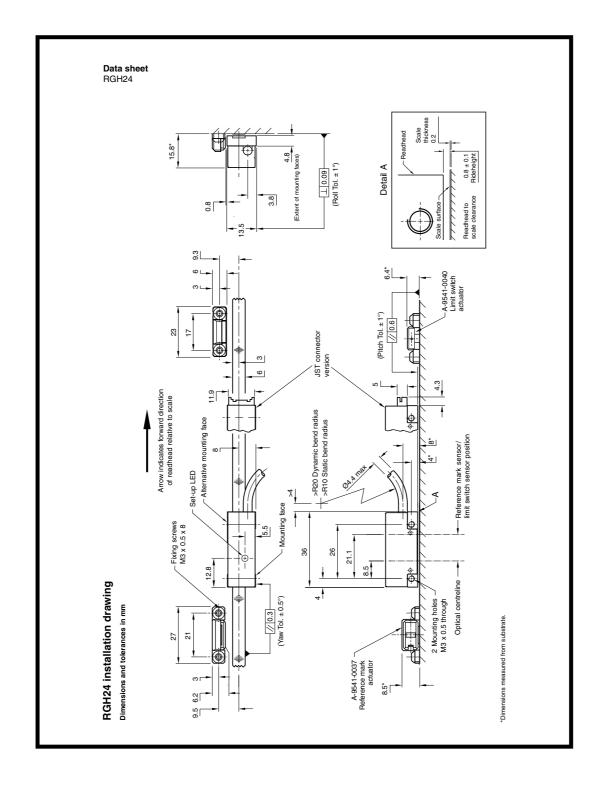
## Doc. 3 Alternativa encoder lineal HEIDENHAIN LF183





## Doc. 4 <u>Alternativas encoder lineal RENISHAW</u>







## Operating and electrical specifications

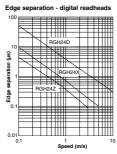
### Clocked outputs

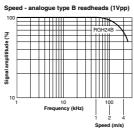
The RGH24W (0.2 µm), RGH24Y (0.1 µm), RGH24H (50 nm), RGH24I (20 nm) and RGH24O (10 nm) readheads have clocked outputs. These are designed to prevent fine edge separations being missed by receiving electronics utilising slower clock speeds. The table below shows the maximum speed and associated minimum recommended counter clock frequency for these readheads.

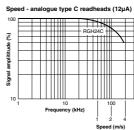
Head type	Maximum speed (m/s)	Minimum recommended counter clock frequency (MHz)
<b>D</b> (5 μm) <b>X</b> (1 μm) <b>Z</b> (0.5 μm)	10 5 3	$\left(\frac{\text{encoder velocity (m/s)}}{\text{resolution ($\mu m$)}}\right)  \text{x 4 safety factor}$

Std. option JST option			Maximum speed (mm/s)					Minimum recommended counter clock frequency
Head type		<b>W</b> (0.2 μm)	<b>Υ</b> (0.1 μm)	<b>H</b> (50 nm)	(20 nm)	<b>O</b> (10 nm)	(MHz)	
	30	35	-	700	350	130	65	12
	31	36	-	500	250	90	45	8
	32	37	700	-	-	-	-	6
	33	38	500	250	120	40	20	4

NOTE: Maximum speeds of clocked output variants assume 3 m maximum cable length and minimum 5 V supply at readhead connector.



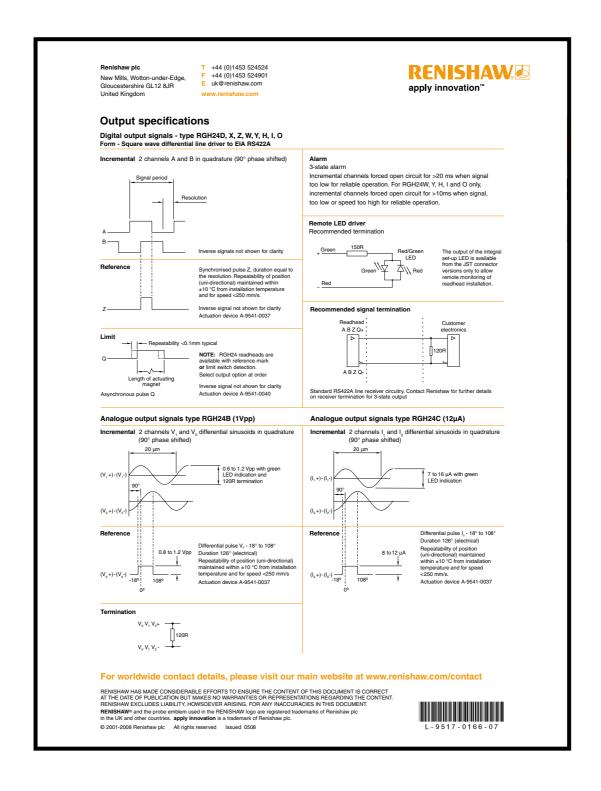




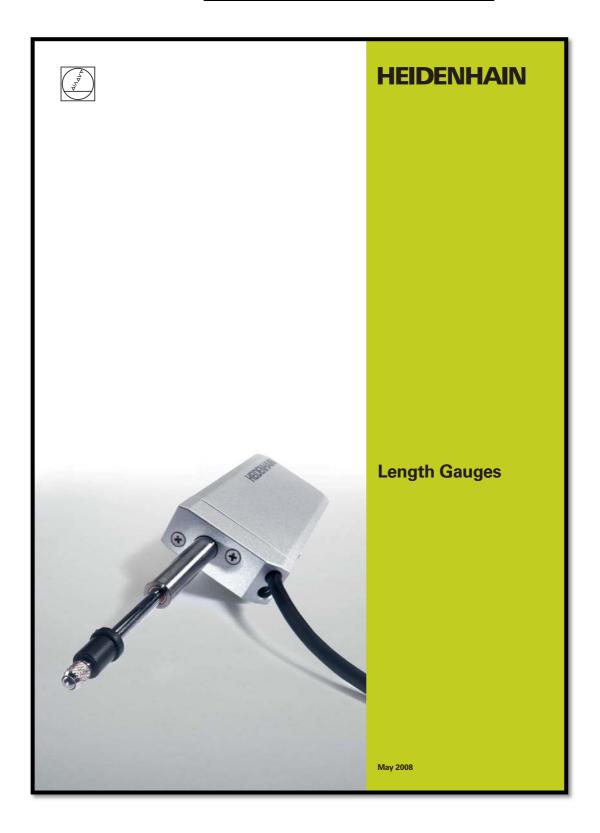
5 V± 5% Ripple

120 mA 200 mVpp maximum @ frequency up to 500 kHz maximum NOTE: For digital outputs, current consumption figures refer to unterminated readheads. A further 25 mA per channel pair (eg A+, A-) will be drawn when terminated with 120  $\Omega$ . For analogue type B readheads, a further 20 mA will be drawn when terminated with 120  $\Omega$ . Renishaw encoder systems must be powered from a 5 V dc supply complying with the requirements for SELV of standard EN (IEC) 60950.

Storage -20 °C to +70 °C Operate	ting 0 °C to +55 °C			
Storage 95% maximum relative humidity (non-condensing) Operating 80% maximum relative humidity (non-condensing)				
IP40				
Operating 500 m/s <sup>2</sup> BS EN 60068-2-7:1993 (IEC 68-2-7:1983)				
1000 m/s², 6 ms, ½ sine BS EN 60068-2-27:1993 (IEC 68-2-27:1987)				
100 m/s² max @ 55 Hz to 2000 Hz BS EN 60068-2-6:1996 (IEC 68-2-6:1995)				
Readhead 11 g Cable 34 g/m				
BS EN 61000 BS EN 55011				
Double-shielded maximum diameter 4.4 mm cable. Flex life >20 x 10 <sup>6</sup> cycles at 20 mm bend radius				
Code - connector type A - 9 pin D type plug C - 9 pin circular plug D - 15 pin D type plug L - 15 pin D type plug F - Flying lead Z - JST Connector	Application All readheads RGH24C RGH24D, X, Z, W, Y, H, I, O RGH24B All readheads RGH24D, X, Z, W, Y, H, I, O			
The RGH24 JST connector series readheads have been designed to the relevant EMC standards but must be correctly integrated to achieve EMC compliance. In particular attention to shielding and earthing arrangements is critical. Renishaw recommends the use of a double screened cable as used in the cable variants of the RGH24. Refer to RGH24 readhead installation guide for electrical connection information for these readheads.				
	Storage 95% maximum relative hur Operating 80% maximum relative hur Operating 80% maximum relative hur IP40  Operating 500 m/s² BS EN 60068  1000 m/s², 6 ms, ½ sine BS EN 6  100 m/s² max @ 55 Hz to 2000 Hz  Readhead 11 g Cable 34 g/m  BS EN 61000 BS EN 55011  Double-shielded maximum diamete  Code - connector type A - 9 pin D type plug C - 9 pin circular plug D - 15 pin D type plug L - 15 pin D type plug F - Flying lead Z - JST Connector  The RGH24 JST connector series is standards but must be correctly intratention to shielding and earthing :			



Doc. 5 Palpador lineal HEIDENHAIN-SPECTO ST1288



# **Principle of Function**

HEIDENHAIN length gauges are characterized by long measuring ranges and consistently high accuracy. The basis for both is the measuring principle of photoelectrically scanning an incremental scale.

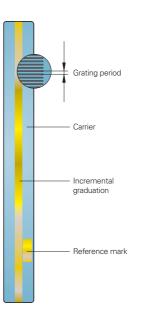
HEIDENHAIN linear encoders use material measuring standards consisting of incremental graduations on substrates of glass or glass ceramic. These measuring standards permit large measuring ranges, are insensitive to vibration and shock, and have a defined thermal behavior. Changes in atmospheric pressure or relative humidity have no influence on the accuracy of the measuring standard—which is the prerequisite for the high long-term stability of HEIDENHAIN length gauges.

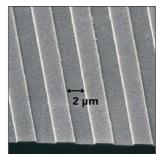
The masters for these graduations are fabricated on dividing engines developed and built by HEIDENHAIN. High thermal stability during the manufacturing process ensures that the graduations have **high accuracy** over the measuring length. The master graduation is applied to the carrier using the DIADUR copying process developed by HEIDENHAIN, which produces very thin but durable graduation structures of chromium.

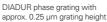
The incremental graduation is **photo-electrically scanned** without mechanical contact and therefore without wear. Light passes through the structured scanning reticle and over the scale onto photo-voltaic cells. The photovoltaic cells produce sinusoidal output signals with a small signal period. Interpolation in the subsequent electronics makes very small measuring steps into the nanometer range possible. The scanning principle, together with the extremely fine graduation lines and their high edge definition ensure the quality of the output signals as well as the **small position error within one signal period.** This applies particularly to HEIDENHAIN length gauges, which use a DIADUR phase grating as measuring standard. The interferential scanning method produces sinusoidal incremental signals with a period of only 2 µm.

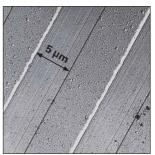
### Reference mark

Photoelectric scanning of grid structures results in an incremental, i.e. counting, measurement. To ascertain positions, an absolute reference is required. The reference mark enables the exact reestablishment of the most recently defined datum, for example after an interruption in power. It is photoelectrically scanned and is permanently associated with exactly one measuring step, regardless of the direction or velocity of traverse.









DIADUR scale

# **Mechanical Design**

HEIDENHAIN length gauges function according to the **Abbe measuring principle,** i.e. the measuring standard and the plunger are exactly aligned. All components comprising the **measuring loop**, such as the measuring standard, plunger, holder and scanning head are designed in terms of their mechanical and thermal stability for the highest possible accuracy of the length gauge

HEIDENHAIN length gauges have a defined **thermal behavior**. Since temperature variations during measurement can result in changes in the measuring loop, HEIDENHAIN uses special materials with low  $\alpha_{\text{therm}}$  coefficients of expansion for the components of the measuring loop. the components of the measuring loop, for example in the CERTO length gauges. The scale is manufactured of Zerodur ( $\alpha_{therm} \approx 0 \text{ K}^{-1}$ ), and the plunger and holder are of Invar ( $\alpha_{therm} \approx 1 \cdot 10^{-6} \text{ K}^{-1}$ ). This makes it possible to guarantee its high measuring accuracy over a relatively large temperature range.

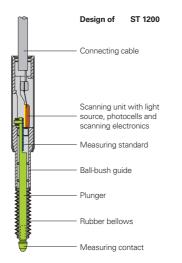
Length gauges from HEIDENHAIN have a sturdy design. Even high vibration and shock loads have no negative influence on the accuracy.

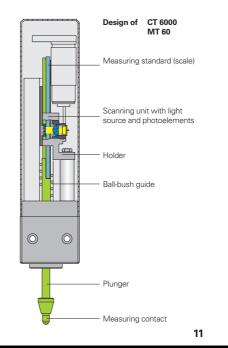
The ball-bush guided plunger tolerates high radial forces and moves with very low friction. It has an M2.5 thread to hold measuring contacts.

Parts subject to wear HEIDENHAIN length gauges contain components that are subject to wear, depending on the application and manipulation. These include in particular the following parts:

- LED light source
  Guideway (tested for at least 5 million strokes\*)
  • Cable link for CT, MT 60 and MT 101
- (tested for at least 1 million strokes\*)
- · Scraper rings
- Rubber bellows on ST 1200
- \* On CT, MT 60 M and MT 101 M only with actuation by switch box

DIADUR is a registered trademark of DR. JOHANNES HEIDENHAIN GmbH, Traunreut, Germany. Zerodur®is a registered trademark of Schott-Glaswerke, Mainz, Germany.





# **Measuring Accuracy**

The accuracy of position measurement with length gauges is mainly determined by the following factors:

• The quality of the graduation

- The quality of the scanning process
  The quality of the signal processing electronics
  • The error from the scale guideway
- relative to the scanning unit

A distinction is made between position error over relatively large paths of traverse—for example the entire measuring range—and that within one signal period.

## Position error over the measuring range

Length gauge accuracy is specified as system accuracy, which is defined as follows:

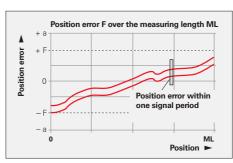
The extreme values of the **total error F** with reference to their mean value—lie over the entire measuring length within the system accuracy ± a. They are measured during the final inspection and documented in the calibration chart.

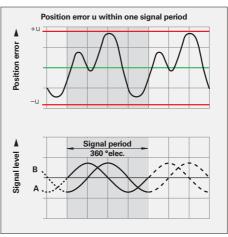
# Position error within one signal period The position error u within one signal

period is determined by the signal period of the length gauge, as well as the quality of the graduation and its scanning. At any position over the entire measuring length, it does not exceed approx. ± 1 % of the signal period.

The smaller the signal period, the smaller the position error within one signal period. In the calibration chart of the HEIDENHAIN-CERTO, this position error within one signal period is shown as a tolerance band.

	Signal period of the scanning signals	Max. position error u within one signal period
CT 2500 CT 6000	2 μm	Approx. ± 0.02 μm
MT 1200 MT 2500	2 μm	Approx. ± 0.02 μm
MT 60 MT 101	10 µm	Approx. ± 0.1 μm
ST 1200 ST 3000	20 μm	Approx. ± 0.2 μm
12	ı	I





All HEIDENHAIN length gauges are inspected before shipping for accuracy and proper function.

They are calibrated for accuracy during retraction and extension of the plunger. For the HEIDENHAIN-CERTO, the number of measuring positions is selected to ascertain very exactly not only the long-range error, but also the position error within one signal period.

The Manufacturer's Inspection
Certificate confirms the specified system
accuracy of each length gauge. The
calibration standards ensure the
traceability—as required by EN ISO 9001—
to recognized national or international
standards.

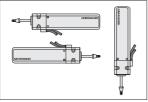
For the HEIDENHAIN-METRO and HEIDENHAIN CERTO series, a calibration chart documents the position error over the measuring range. It also shows the measuring step and the measuring uncertainty of the calibration measurement.

For the HEIDENHAIN-METRO the calibration chart shows the mean value of one forward and one backward measuring stroke.

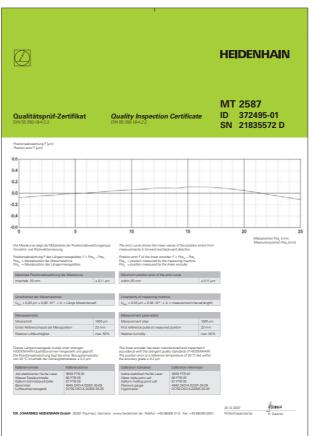
The HEIDENHAIN-CERTO is represented in the calibration chart as the envelope curve of the measured error. The HEIDENHAIN-CERTO length gauges are supplied with two calibration charts, each for different operating attitudes.



Operating attitude for calibration chart 1



Operating attitude for calibration chart 2



Example

## Temperature range

The length gauges are inspected at a reference temperature of 20 °C. The system accuracy given in the calibration chart applies at this temperature. The operating temperature range indicates the ambient temperature limits between which the length gauges will function properly. The storage temperature range of –20 °C to 60 °C applies for the unit in its packaging.

# **Gauging Force—Plunger Actuation**

**Gauging force**Gauging force is the force that the plunger exercises on the measured object. An excessively large gauging force can cause deformation of the measuring contact and the measured object. If the gauging force is too small, an existing dust film or other obstacle may prevent the plunger from fully contacting the measured object. The gauging force depends on the type of

**Plunger actuation by spring** For the MT 12x1, MT 25x1, ST 12x8 and ST 30x8, the integral spring extends the plunger to the measuring position and applies the **gauging force**. In its resting position, the plunger is extended. The gauging force depends on:

The operating attitude

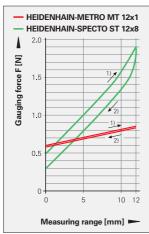
- The plunger position, because the gauging force changes over the measuring range
  The measuring direction, i.e., whether the gauge measures with extending or refrection plunger. retracting plunger

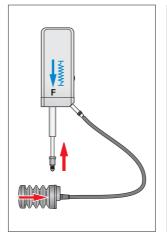
There are several ways of actuating the length gauge plunger:

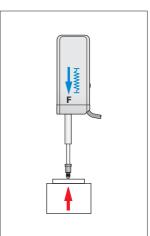
**Plunger actuation by cable-type lifter** Through a cable mechanism, the plunger is retracted by hand and then extended onto the measured object. The measurement is made with extending plunger.

# Plunger actuation by measured object The complete length gauge is moved

relative to the measured object. The measurement is made with retracting







1) Plunger retraction 2) Plunger extension

Pneumatic plunger actuation
The pneumatically actuated plungers of the
MT 1287, MT 2587, ST 12x7 and ST 30x7
length gauges are extended by the application of compressed air. When the air connection is ventilated, the integral spring retracts the plunger to a protected resting position within the housing.

The gauging force can be adjusted to the measuring task through the level of air pressure. At constant pressure, it depends on the operating attitude and the plunger position. The vertically downward position with retracted plunger, for example, has the greatest gauging force, and the vertically upward position with extended plunger the lowest. The data given in the specifications are approximate and are subject to variation due to tolerances and to wear in the seal.

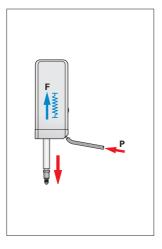
The length gauges with pneumatic plunger actuation are particularly well suited for automated measuring systems.

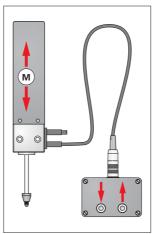
Motorized plunger actuation The CT 2501, CT 6001, MT 60 M and MT 101 M length gauges feature an integral motor that moves the plunge. It is operated through the switch box either by push button or over the connection for external operation. The plungers of the CT 2501, CT 6001, and MT 60M length gauges must not be moved by hand if the switch box is connected.

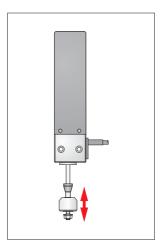
The **gauging force** of the CT 2501, CT 6001, and MT 60 M motorized length gauges is adjustable in three stages through the switch box. The force remains constant over the measuring range but depends on the operating attitude. Regardless of the operating attitude—whether it measures vertically downward (with the SG 101V switchbox) or horizontally (with the SG 101 H switch box)—the MT 101 M exercises a constant gauging

Switch box and power adapter (only with MT101 M) must be ordered separately.

External plunger actuation by coupling For the CT 2502, CT 6002, MT 60 K, MT 101 K and special versions "without spring" of the MT 1200 and MT 2500, the plunger is freely movable. For position measurement, the plunger is connected by a coupling with a moving machine element. The force needed to move the plunger is specified as the required moving force. It depends on the operating







# Mounting

In addition to the length gauge itself, the mechanical design of the measuring setup also plays a role in defining the quality of measurement.

### Abbe principle

HEIDENHAIN length gauges enable you to work according to the Abbe measuring principle: The measured object and scale must be in alignment to avoid additional measuring error.

### Measuring loop

All components included in the measuring loop such as the holder for the measured object, the gauge stand with holder, and the length gauge itself influence the result of measurement. Expansion or deformation of the measuring setup through mechanica or thermal influences adds directly to the error.

### Mechanical Design

A stable measuring setup must be ensured. Long lateral elements within the measuring loop are to be avoided. HEIDENHAIN offers a stable gauge stand as an accessory. The force resulting from the measurement must not cause any measurable deformation of the measuring loop. Incremental length gauges from HEIDENHAIN operate with small gauging force and have very little influence on the measuring setup.

## Thermal behavior

Temperature variations during measurement cause changes in length or deformation of the measuring setup. After a change in temperature of 5 K, a steel bar of 200 mm length expands by 10 µm.

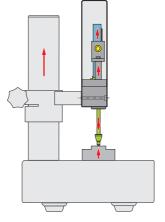
Length changes resulting from a uniform deviation from the reference temperature can largely be compensated by resetting the datum on the measuring plate or a master; only the expansion of the scale and measured object go into the result of measurement. Temperature changes during measurement cannot be ascertained mathematically.

For critical components, HEIDENHAIN therefore uses special materials with low coefficients of expansion, such as are found in the HEIDENHAIN-CERTO gauge stand. This makes it possible to guarantee the high accuracy of HEIDENHAIN-CERTO even at ambient temperatures of 19 °C to 21 °C and variations of  $\pm$  0.1 K during measurement.



## The measuring loop:

All components involved in the measuring assembly, including the length gauge



## Thermally induced length change

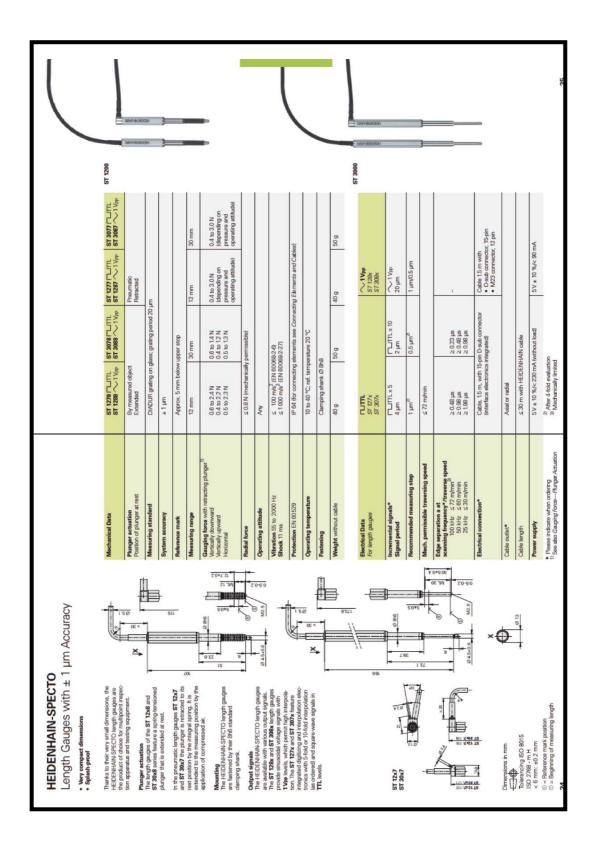
Expansion of the measuring loop components as a result of heat

### Acceleration

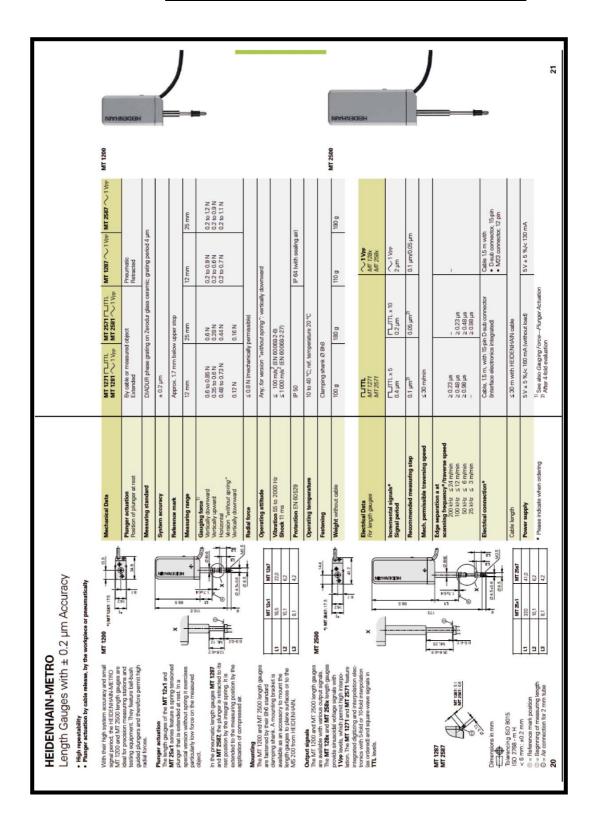
Shock and vibration of any kind is to be avoided during measurement so as not to impair the high accuracy of the length gauge.

The maximum values given in the specifications apply to the effect of external acceleration on the length gauge. They describe only the mechanical stability of the length gauge, and imply no guarantee of function or accuracy.

In the length gauge itself, unchecked extension of the spring-driven or non-coupled moving plunger can cause high acceleration onto the measured object or measuring plate surface. For the MT 1200 and MT 2500 series length gauges, use the cable-type lifter whenever possible (see *Accessories*). The cable lifter features adjustable pneumatic damping to limit the extension velocity to a non-critical value.



# Doc. 6 Alternativa palpador lineal HEIDENHAI-METRO MT1281



### Doc. 7 Alternativa palpador MARPOSS HBT 3441557005



## LÍNEA DE CABEZAS LÁPIZ

La línea de cabezas lápiz RED CROWN\* ha sido desarrollada por TESTAR una División de MARPOSS, para resolver las exigencias de control de calidad en ambiente de taller, se presentan en 4 variantes

## Línea base:

Presenta 52 modelos standard con un campo de medida comprendido entre ± 0,5 mm y ± 5 mm. Las cabezas lápiz están disponibles con transductor LVDT (puente entero) o HBT (medio puente) calibrado para su conexión a las unidades electrónicas de visualización TES-TAR E18, E4, E4N, Quick Read Microcolumna y mediante el sistema de adquisición de datos Easy Box™ o Gage-Box™ a una Central de Medida E9066s™

### Línea compatible:

Una línea completa de cabezas lápiz con campo de medida standard TESTAR, do-tadas del conector eléctrico adecuado y tarado para su conexión a la unidad elec trónica que se disponga.

## Línea sin conector:

Los 52 modelos de la línea base pueden ser suministrados sin conector. Sobre la base de las características eléctricas específicas para cada cabeza, el usuario puede montar el conector necesario y realizar la calibración para la electrónica que se disponga.

## Línea Soft-Touch:

Cabezas lápiz proyectadas con fuerza de medida muy baja para la medición del vidrio, tubos de rayos catódicos, parabrisas del automóvil y materiales plásticos. Estas cabezas están disponibles

en la configuración base o compatible.

### Cabezas Iápiz RED CROWN™: la elección más fácil para la medición de cualquier pieza.

La fiabilidad y la duración de las cabezas lápiz está garantizada por los innovativos diseños y la utilización de los materiales apropiados, desarrollados gracias a la experiencia de Testar en el campo del control de calidad.

Con la utilización de las cabezas lápiz Red Crown™ se garantiza una gran precisión de la medida, incluso inferior a la micra, mejorando la calidad de los da-tos de medida y su elaboración estadís-

El programa Red Crown ofrece:

- Gama completa de modelos stan-
- dards y compatibles Gran calidad y precisión
- Precio competitivo Corto plazo de entrega · Larga duración

## GARANTÍA DE CALIDAD

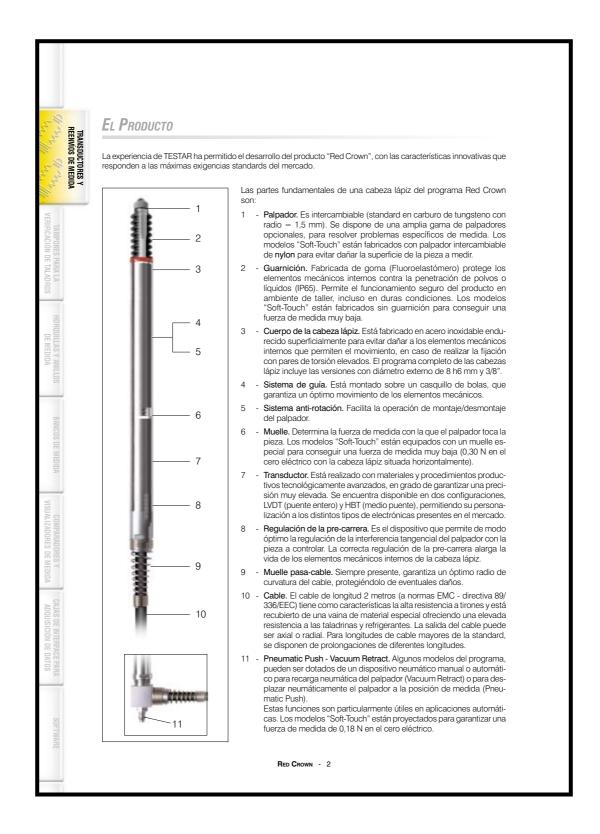
El personal técnico TESTAR goza de una gran experiencia en la fabricación y la aplicación de las cabezas lápiz, en las soluciones propias y en las de terceros. La experiencia obtenida en el ambiente productivo de taller, ha sido fundamental para desarrollar el nuevo programa RED CROWN™. TESTAR, certificada ISO 9000, fabrica cada una de las cabeza lápiz realizando un severo test de calidad, fruto de la experiencia y de la garantía que un medidor de calidad debe ofrecer. El producto se controla al 100%, siguiendo procedimientos internacional-mente reconocidos y utilizando equipos automáticos que definen sus características fundamentales

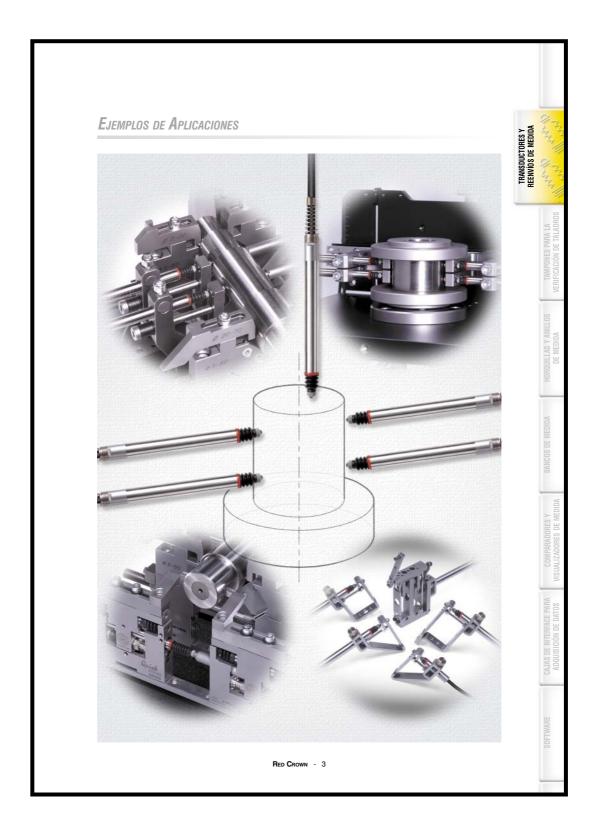


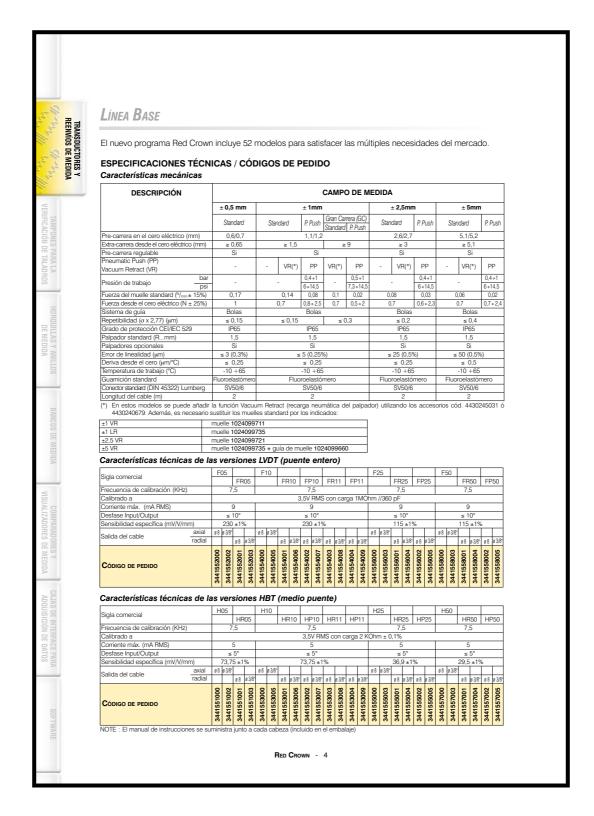


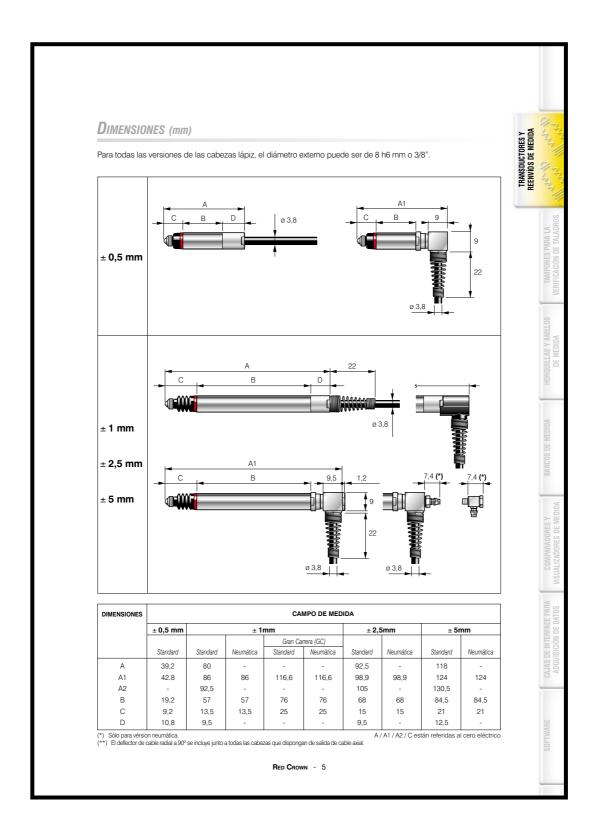












# LÍNEA COMPATIBLE

TESTAR ha desarrollado una línea de modelos Red Crown con el conector y el tarado necesario, que permiten ser utilizadas en sustitución de cabezas de otros fabricantes. Esto permite al usuario, aprovecharse de la tecnología utilizada por el producto Red Crown, sin tener que sustituir la electrónica existente. Las características técnicas y las dimensiones de estas cabezas son las mismas que los modelos correspondientes a la Línea Base. La línea compatible está en continuo desarrollo, por lo que pueden consultar la lista actualizada con los correspondientes códigos, en la página web www.testar.com.

		CAMPO DE MEDIDA									
Modelos Base			± 0,5 mm		± 1 mm		± 1 mm Gran Carrera	± 2,5 mm		± 5 mm	
FABRICANTE	Tipo Trans	Ø	H05	HR05	H10	HR10	HR11	H25	HR25	H50	HR50
TESA	Medio puente (HBT)	8	3441561000	3441561001	3441561002	3441561003 (*)	3441561005 (*)	3441561007	3441561008 (*)	3441561010	3441561011 (*)
MERCER		8	3441564000	3441564001	3441564002	3441564003 (*)	3441564005 (*)	3441564007	3441564008 (*)	3441564010	3441564011 (*)
МЕТЕМ		8	3441569000	3441569001	3441569002	3441569003 (*)	3441569005 (*)	3441569007	3441569008 (*)	3441569010	3441569011 (*)
METREL		8	3441563000	3441563001	3441563002	3441563003 (*)	3441563005 (*)	3441563007	3441563008 (*)	-	-
MAHR-FEINPRUEF		8	3441567000	3441567001	3441567002	3441567003 (*)	3441567005 (*)	3441567007	3441567008 (*)	3441567010	3441567011 (*)
NOVIBRA		8	-	-	3441568003	-	-	-	-	-	-
MACHSIZE-SYSTEM E		8	3441562009	3441562010	3441562008	3441562011	3441562013	-	-	-	-
AIR GAGE		3/8"	3441562000	3441562001	3441562002	3441562003 (*)	-	3441562005	3441562006 (*)	-	-
FABRICANTE	Tipo Trans	Ø	F05	FR5	F10	FR10	FR11	F25	FR25	F50	FR50
ETAMIC (ZDB)	Puente entero (LVDT)	8	3441565009	3441565010	3441565006	3441565011	3441565013	3441565007	3441565015	3441565008	3441565017

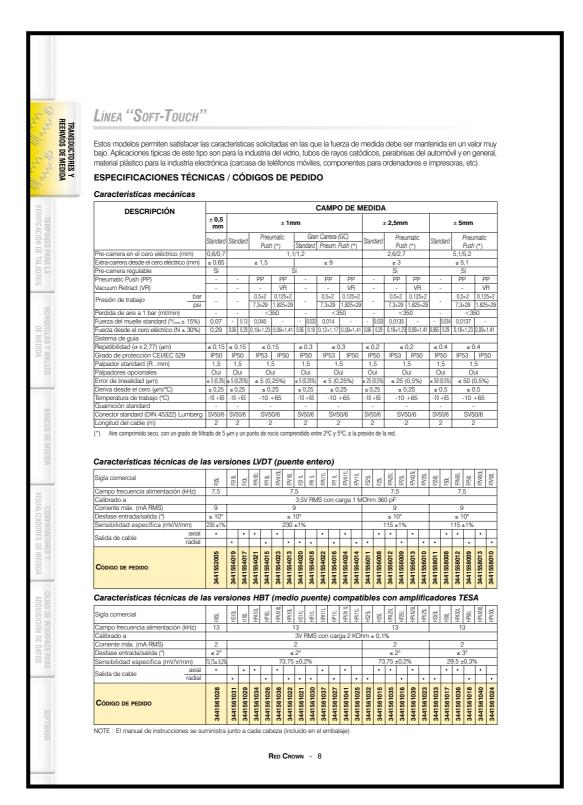
(\*) En estos modelos se puede añadir la función Vacuum Retract (recarga neumática del palpador) utilizando los accesorios cód. 4430245031 ó 4430240679. Es necesario, asimismo, sustituir el muelle estándar por el indicado en la tabla de la página 4.

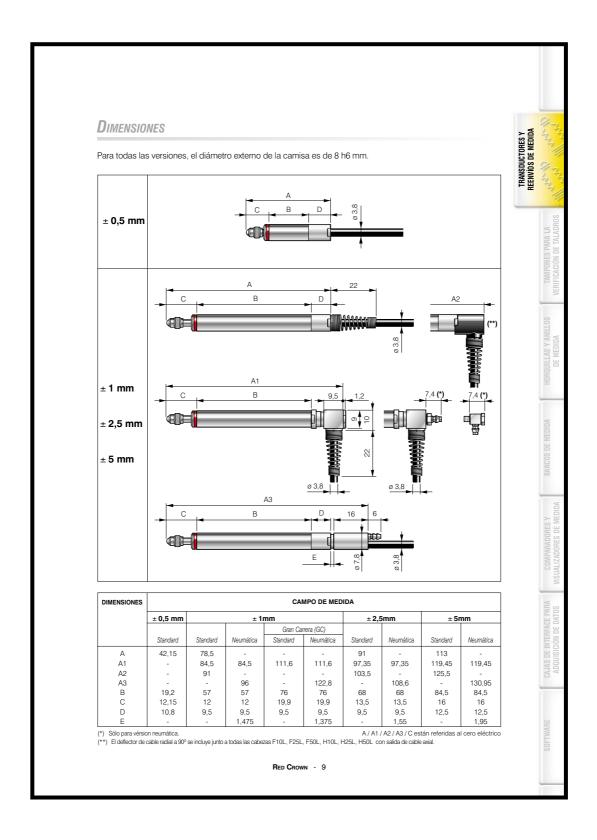
Modelos Pneumatic Push		CAMPO DE MEDIDA								
		± 1 mm	± 1 mm Gran Carrera	± 2,5 mm	± 5 mm					
FABRICANTE	Tipo Trans	Ø	HP10	HP11	HP25	HP50				
TESA	Medio puente (HBT)	8	3441561004	3441561006	3441561009	3441561012				
MERCER		8	3441564004	3441564006	3441564009	3441564012				
МЕТЕМ		8	3441569004	3441569006	3441569009	3441569012				
METREL		8	3441563004	3441563006	3441563009	-				
MAHR-FEINPRUEF		8	3441567004	3441567006	3441567009	3441567012				
MACHSIZE-SYSTEM E		8	3441562012	3441562014	-	-				
AIR GAGE		3/8"	3441562004	-	3441562007	-				
FABRICANTE	Tipo Trans	Ø	FP10	FP11	FP25	FP50				
ETAMIC (ZDB)	Puente entero (LVDT)	8	3441565012	3441565014	3441565016	3441565018				

NOTE : El manual de instrucciones se suministra junto a cada cabeza (incluido en el embalaje)

RED CROWN - 6

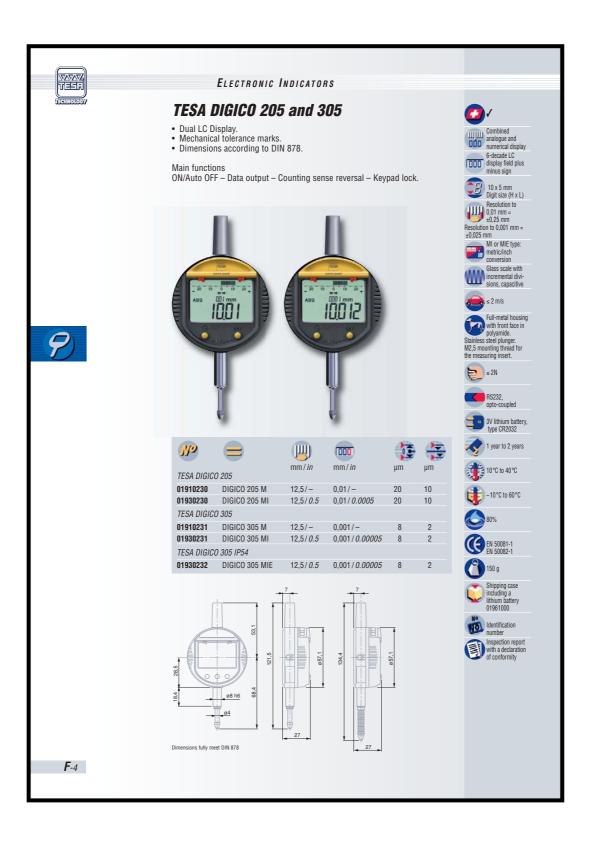
### LÍNEA SIN CONECTOR TRANSDUCTORES Y REENVIOS DE MEDIDA ESPECIFICACIONES TÉCNICAS / CÓDIGOS DE PEDIDO Características mecánicas CAMPO DE MEDIDA ± 0,5 mm DESCRIPCIÓN Standard Standard Standard Standard Standard P. Push Push Push 0,6/0,7 ≥ 0,65 Oui Pre-carrera en el cero eléct Extra-carrera desde el cero e Pre-carrera regulable Pneumatic Push (PP) VR(\*) VR(\*) PP VR(\*) PP PP VR(\*) 0.4 +1 0.4+1 Presión de trabaio 6+14,5 0,03 uerza del muelle standard (N/mm ± 15%) uerza desde el cero eléctrico (N ± 25%) 0,6+2 bolas ≤ 0,15 IP65 Grado de guía Repetibilidad (σ x 2,77) (μm) Grado de protección CEI/IEC 529 Palpador standard (R...mm) Palpadores opcionales bola bolas bola IP65 Fluoroelastómer 3,5 (\*) En estos modelos se puede añadir la función Vacuum Retract (recarga neumática del palpador) utilizando los accesorios cód. 4430245031 ó 4430240679. Es necesario, asimismo, sustituir el muelle estándar por el indicado en la tabla de la página 4. Características técnicas de las versiones LVDT (puente entero) F05 FR05 152+ 248 ≤ 2,7 (0,3%) 2+ 20 1+ 7 FR10 FP10 FR11 FP11 0 FR50 FP50 114+ 122 ≤ 38 (0,4%) 4+ 9 Sensibilidad específica (mV/mm/V) Error de linealidad (μm) Campo frecuencia alimentación (kHz) Campo tensión alimentación (Vms) Campo absorción corriente aliment (mAV) Desfase entrada/salida (°) 3,2÷ 0,5 10÷ -8 -3,3÷ -8,4 Jestase entrada/salida (\*) recuencia desfase del cero (kHz) Zarga calibración (kΩ) recuencia de test (kHz) ensión alimentación de test (Vrms) Carga de test Sensibilidad condición de test (mV/mm/V). Linealidad condición de test (µm) Absorción corriente condición de test (mAV) Desfase entrada/salida condición de test (%) 1 MΩ//360 pF 1 MΩ//360 pF 1 MΩ//360 pF 1 MΩ//360 pF 240 ±5% ≤ 3 (0,3%) 239 ±5% ≤ 2 (0,1%) 118 ±5% ≤ 25 (0,5%) 116 ±5% ≤ 50 (0,5%) alida del cable CÓDIGO DE PEDIDO Características técnicas de las versiones HBT (medio puente) H05 HR05 H10 HR10 HP10 HR11 HP11 Sensibilidad específica (mV/mm/V) Error de linealidad (μm) Campo frecuencia alimentación (kHz) Campo tensión alimentación (Vrms) Campo absorción coriente aliment. (mAV) 70+87 ≤ 2,5 (0,3%) 2+20 2+5 1,8+0,2 2÷ 5 2,1÷ 0,3 Desfase entrada/salida (°) Frecuencia desfase del clero (kHz) Carga calibración (kΩ) 16÷ -11 uencia de test (kHz arga de test (kΩ) ensibilidad condición test (mV/mm/V) nealidad condición test (μm) CÓDIGO DE PEDIDO NOTE: El manual de instrucciones se suministra junto a cada cabeza (incluido en el embalaje) RED CROWN - 7





### Reloj comparador altura corona TESA DIGICO 305M





# **ANEXO III: Planos**

En este anexo se incluyen todos los planos de las piezas de nueva fabricación o en su defecto de modificación definidas en el proyecto para el montaje y puesta en marcha de la máquina con los nuevos componentes de medida.

Los planos que podemos encontrar son los siguientes:

PLANO 01.02	GUIA CARRO PORTA-SINFÍNA	<u>-85</u>
PLANO 01.07	ALTERNATIVA GUIA CARRO PORTA-SINFÍNA	<u> -87</u>
PLANO 02.17	SOPORTE NUEVO REDUCTOR FAULHABERA	\- <u>89</u>
PLANO 02.19	SISTEMA BLOQUEO CARRO PORTA-SINFÍNA	\- <u>91</u>
PLANO 02.20	CASQUILLO CALCE NUEVO REDUCTORA	<u>-93</u>
PLANO 08.01	MODIFICACION PLACA SOPORTE ENCODER LINEALA	<u> 1-95</u>
PLANO 08.05	CARRO RODAMIENTO LINEALA	<u>-97</u>
PLANO 08.07	CALCE ENCODER LINEALA	<u>-99</u>
PLANO 08.08	MODIFICACION PIEZA UNION ENCODER A CARROA-	101

